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Facultad de Química

Mujica

Estudio sobre las Propiedades Electrónicas de Aleaciones

T E S I S

Que para obtener el título de:

Q U I M I C O

p r e s e n t a :

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LAT indica el tipo de malla, sus posibles valores son:

LAT = 1	FCC
LAT = 2	BCC
LAT = 3	Diamante
LAT = 4	HCP
LAT = 5	Estructuras Especiales
LAT = 6	Aleaciones

- (JRI(JJ),JJ=1,NJJ) FORMATO(6F10.6)

JRI punto de la malla de APW(malla creada y descrita en CRYs) correspondiente al radio de la esfera.

- OMA, A, C, XALPHA FORMATO(6F10.6)

OMA volumen por átomo(unidades atómicas)³ :

A, C parámetros de la malla(u. a.). En el caso de aleaciones y estructuras especiales A y C pueden ser=1.0 dependiendo de la forma en que se den las distancias.

XALPHA parámetro de intercambio cuando XALPHA no se especifica (XALPHA=0), el cálculo se efectua con los valores de $\alpha=2/3$ y $\beta=0.003$; de lo contrario $\alpha=XALPHA$.

En el caso de aleaciones o de estructuras especiales se leen dentro de un DO de JJ=1,NJJ los siguientes datos:

- (XNA(I,JJ), I=1,14) FORMATO(8F10.6)

- (AAD(I,JJ), I=1,14) FORMATO(8F10.6)

XNA es el número de vecinos en cada capa; si LAT=5 será para las primeras 14 capas, si LAT=6 se da el número de vecinos de las 7 primeras capas del tipo del átomo central y de 8-14 el número de vecinos del otro tipo de átomo en éstas 7 capas.

Se lee primero cuando el átomo de tipo 1 es el central y luego cuando el átomo de tipo 2 es el central.

AAD son las distancias para cada capa de vecinos y se dan de la misma forma que XNA. Cuando es una aleación, la primera distancia para el átomo que no es el central debe de ser diferente de cero.

- MAXL, NE, ZVAL(1), ZVAL(2), NUMA(1), NUMA(2), BE, ES, DVINT(1), DVINT(2), IRESIS FORMATO(6I5, 4F10.5, 2I5)

MAXL máximo momento angular.

NE número de energías para el cálculo de las derivadas logarítmicas y corrimientos de fase, no debe de ser mayor de 60.

ZVAL(1), ZVAL(2) número de electrones de valencia para cada tipo de átomo.

NUMA(1), NUMA(2) número de dispersores de cada tipo de átomo.

BE valor de la energía inicial, BE ≠ 0, por lo general BE = 0.01.

ES intervalo de la malla de energías en LOGDER.
DVINT(1), DVINT(2) potencial intersticial adicional
para cada tipo de átomo.

IRESIS $\neq 0$ solo cuando se quiere calcular la resistividad. Cuando IRESIS $\neq 0$ se lee:

- (AQUP(J), j=1,40) FORMATO(8F10.5)

AQUP tabla de factor de estructura.

Cuando IAL $\neq 0$, o sea que se quiere calcular la densidad de estados se leen las siguientes tarjetas:

- TMAX, LLSS, IOPL, NPP, ATOCEL, NAME

FORMATO(I5,I3,2I2,F8.4,10A6)

TMAX tiempo máximo estimado para el cálculo en segundos.

LLSS $\neq 0$ cuando se quiere variar el valor de LMAX procedente de LOGDER. LSS=(LMAX+1)-LLSS.

IOPL = 1 si se quieren tomar en cuenta para el cálculo los electrones p.

NPP número de puntos para la interpolación, si NPP=0 entonces NPP=4.

ATOCEL número de átomos dentro de la celda con parámetros A y C.

NAME título.

- PARA, EEMIN, EEMAX, EEDELT, FINT1, INUMA(1), INUMA(2)

FORMATO(I5,4F10.5,2I5)

PARA $\neq 0$ cuando se quiere que la máquina perfore el valor de la última energía calculada y

el valor de la integral de la densidad de estados hasta esa energía.

EEMIN corrección para el valor de la energía mínima, si EEMIN \neq 0, EMIN = EEMIN. Si EEMIN = 0 el programa utilizará como energía mínima la última del cálculo anterior, si es el primer cálculo usa la de LOGDER.

EEMAX corrección para el valor de la energía máxima, si EEMAX \neq 0, EMAX = EEMAX.

EEDELT corrección al tamaño del intervalo, si EEDELT \neq 0 EDELT = EEDELT.

FINT1 valor de la integral de la densidad de estados de del que parte la misma. si FINT1 = 0 empieza en 0 la primera vez y las siguientes ocasiones con el valor que guardó.

INUMA(1), INUMA(2) corrección para el número de dispersores para cada tipo de átomo; el número total de dispersores (NUMSC) será:

$$\text{NUMSC} = \text{NUMA}(1) + \text{NUMA}(2) + \text{INUMA}(1) + \text{INUMA}(2).$$

- (LX(I),LY(I),LZ(I),I=1,NUMSC) FORMATO(8F10.7)

Coordenadas para cada uno de los dispersores.

- ((SCF(L,TN),L=1,LSS+1),TN=1,NJJ) FORMATO(8F10.7)

SCF escalamiento de los corrimientos de fase de momento angular 1, se perfora una tarjeta para cada tipo de átomo.

Cuando únicamente se quiere hacer el cálculo de la densidad de estados y se parte de los datos guardados por el programa en disco

se necesitan: la primera tarjeta descrita, se omiten las siguientes hasta la tarjeta donde se lee TMAX, LLSS, etc.

Otra posibilidad es hacer el cálculo de la densidad de estados con corrimientos de fase no obtenidos en LOGDER para lo cual se da el siguiente instructivo, algunas tarjetas solamente se mencionan porque ya fueron descritas.

- ICALL FORMATO(2I5)
- A0, EMIN, EMAX, EDELT, LSS, NPH, T, NUMA(1), ZVAL(1), NUMA(2),
ZVAL(2) FORMATO(4F10.6,7I3)

A0 parámetro de la malla.

EMIN energía mínima, debe de ser diferente de cero.

EMAX energía máxima.

EDELT tamaño del intervalo de malla.

LSS máximo momento angular.

NPH número de corrimientos de fase que tiene que leer el programa.

T número de diferentes tipos de átomos.

NUMA(1), ZVAL(1), NUMA(2), ZVAL(2) ya descritas.

- TMAX, LLSS, IOPL, NPP, ATOCFL, NAME
FORMATO(I5,I3,2I2,F8.4,10A6)
- PARA, EEMIN, EEMAX, EEDELT, FINT1, INUMA(1), INUMA(2)
FORMATO(I5,4F10.5,2I5).
- (LX(I),LY(I),LZ(I),I=1,NUMSC) FORMATO(8F10.7)
- ((SCF(L,TN),L=1,LSS+1),TN=1,T) FORMATO(8F10.8)
- ((E(I,TN),E(I+1,TN),E(I+2,TN),E(I+3,TN),E(I+4,TN),E(I+5,TN),
E(I+6,TN),E(I+7,TN),I=1,NPH,8),TN=1,T)
FORMATO(8F10.8)

energía correspondiente a cada corrimiento de fase.

- ((PH(L,I,TN),PH(L,I+1,TN),PH(L,I+2,TN),PH(L,I+3,TN),PH(L,I+4,TN)
PH(L,I+5,TN), PH(L,I+6,TN),PH(L,I+7,TN),L=1,NPH,8),TN=1,T)

FORMATO(8F10.8)

corrimientos de fase.

APENDICE II. DESCRIPCION DE LOS RESULTADOS DEL CALCULO DE LA

ALEACION Fe₄Ge.

Se presentan a continuación los resultados obtenidos en el cálculo de la aleación Fe₄Ge con una estructura FCC.

En la primera hoja se encuentran las distancias del centro a las primeras 14 capas de vecinos para las estructuras FCC, BCC y Diamante, se escriben también el número de vecinos para las estructuras anteriores y para la estructura HCP, las distancias para esta estructura se calculan en el programa.

A continuación se obtiene la tabla de radios de APW y las tablas de densidades electrónicas ya interpoladas a la malla de APW y las integrales de la densidad de carga para cada tipo de átomo. En este cálculo se ha legido al Fe como el átomo de tipo 1 y al Ge de tipo 2. Se encuentra después el tipo de malla (LAT) en este caso se indica con el número 6 por tratarse de una aleación (para otras estructuras ver el instructivo en el apéndice I), en seguida el punto de la malla correspondiente a la esfera de muffin-tin este dato recibe el nombre de JRI y en este caso tiene el mismo valor para los dos tipos de átomos

$$JRI = \frac{\ln R_{MT} + 8.85}{0.05} \quad \dots 29)$$

Se encuentran también el volumen por átomo, los parámetros de la

malla y por último los valores de α y β .

En la siguiente hoja se encuentran las distancias y número de vecinos para las primeras 7 capas de vecinos, primero cuando el Fe es el átomo central, en este caso los siete primeros números corresponden a las distancias que hay del Fe central a las primeras siete capas de Fe y los otros siete corresponden a al distancia que hay del Fe central a las siete primeras capas de Ge, en la misma forma aparecen el número de vecinos; en seguida cuando el Ge es el átomo central los primeros siete datos corresponden a las distancias y el número de átomos de Ge y las otras siete a los del Fe. En esta misma hoja encontramos la integral del potencial en la esfera de muffin-tin, la de $4\pi\rho$, la carga dentro de la esfera, el volumen de las esferas, el potencial de intercambio y el número de átomos de cada tipo considerando en este caso como átomos de tipo 1 a los del tipo del átomo central.

En esta parte el programa inicia el cálculo tomando primero al átomo de tipo 2 como central. Los valores que encontramos a continuación son: RI radio de la esfera de muffin-tin para cada tipo de átomo, como se dijo antes en este caso son iguales, RO es el radio de la esfera obtenido a partir del volumen por átomo, V BOUNDARY que es la integral del potencial final en un volumen por átomo, VINT que es el potencial promedio en la región intersticial (la región entre RI y RO), Z es el número atómico para este tipo de átomo, los dos valores de JRI, el tipo de malla (LAT) y los valores de α y β , la tabla que viene a continuación es la tabla del potencial en el cristal cuando el átomo de tipo 2 es el central

y en la siguiente hoja se encuentra este potencial multiplicado por el radio.

A continuación se encuentran los datos necesarios y los resultados de la subrutina LOGDER. Un vint adicional para esta subrutina que permite cambiar la posición del cero de energía(VINT), LMAX es el valor del máximo momento angular, en este caso no se han incluido electrones de tipo f en el cálculo, el número de energías, la energía inicial y el tamaño del intervalo de energías. A continuación aparecen las derivadas logarítmicas para cada l y los corrimientos de fase, la siguiente tabla CEP es

$$CEP_l = \tan \eta_l - \frac{n_l}{j_l} \quad \dots 30)$$

donde n_l y j_l son las funciones de Neumann y Bessel respectivamente.

Al final de esta tabla se encuentra el nivel de Fermi, el número de electrones de valencia para el átomo de tipo 2 y el valor del corrimiento de fase s, p, d al nivel de Fermi.

A continuación se tiene la gráfica de corrimientos de fase vs. energía. La línea formada por * representa al corrimiento de fase de tipo s, la línea de + al de tipo p y la línea formada por - al de tipo d que en este caso es muy pequeño. La línea punteada vertical es el nivel de Fermi.

En la siguiente hoja se obtienen los resultados del cálculo cuando el átomo de tipo 1 es el central, se encuentra también el potencial, el potencial por el radio, aquí como se mencionó en la pag. 7 es importante checar que el potencial intersticial (VINT)

no difiera en mas de 10^{-2} Ry del obtenido para el átomo de tipo 2. En seguida se obtienen los resultados de la subrutina LOGDER, en este caso además se obtiene un nivel de Fermi aproximado para la aleación, promediando los niveles de Fermi de cada tipo de átomo. En la gráfica se puede apreciar la resonancia d para el Fe.

En seguida se encuentran los datos necesarioa y resultados de la subrutina ASIL. En este caso se presenta el cálculo con solo 2 dispersores para poder mostrar una gráfica de la densidad de esta dos completa. La gráfica presentada en el cap. III se obtuvo haciendo el cálculo con 6 dispersores, pero ese cálculo se tuvo que efectuar en varias etapas.

Primero encontramos todos los datos que se le dieron a esta subrutina, como son l_{\max} , el número de diferentes tipos de átomos, el número de átomos por celda, el parámetro de malla y el número de puntos para la interpolación. Esta parte del programa puede no tomar en cuenta a los electrones p para el cálculo, aunque en este caso si se incluyen por tener una contribución importante en el Ge. Se encuentra después la enrgía mínima y máxima y el tamaño del intervalo, los escalamientos s, p, d. Para el átomo de tipo 1 los electrones de valencia y el número de dispersores de este tipo y los corrimientos de fase, a continuación los escalamientos para el átomo de tipo 2, el número de electrones de valencia y el número de dispersores de este tipo y sus corrimientos de fase. Se tienen después las coordenadas de cada dispensor, primero las del átomo de tipo 1 y luego del tipo 2. En este caso con dos dispersores se consideró un dispensor de cada tipo. En seguida encontramos los resultados de la subrutina ASIL que son la densidad de estados, la

contribución de electrones libres, el cambio en la densidad de estados y la densidad integrada de estados que como se mencionó en la descripción de la subrutina nos permite calcular el nivel de Fermi, como podemos observar en este caso el nivel de Fermi se encontró a una energía de 0.985Ry. La densidad de estados y la parte de electrones libres se encuentran representados en la gráfica que aparece a continuación. En esta gráfica la curva formada por * representa a la parte de electrones libres y la curva formada por + a la densidad de estados, la línea punteada vertical nos indica el nivel de Fermi, en este caso encontramos como punto importante un mínimo en la densidad de estados y el nivel de Fermi muy cerca de este, como se puede ver el fig. 5 del cálculo con 6 dispersores el nivel de Fermi se acerca mas al mínimo de la densidad de estados ya que la concentración se asemeja mas a la de formación del vidrio metálico y concuerda mejor con los resultados obtenidos con el modelo de electrones casi libres mencionado en el cap. III.

Abajo de la gráfica encontramos los valores para la suma de Friedel y la densidad de estados por volumen X 100, los números que no tienen paréntesis corresponden a los valores de confianza (faithful).

Cuando se efectua el cálculo de la densidad de estados aparece al principio del programa una serie de resultados que por seguir el orden en el que se efectua el cálculo aquí describimos e incluimos al final. Los valores que encontramos aquí para cada energía son: el valor de la matriz k para cada l y el corrimiento de fase correspondiente, el valor de la parte real y la parte ima ginaria del determinante que como se vió en el capítulo II nos

permite calcular la densidad de estados, cuyo valor también aparece por unidad de volumen y multiplicado por 100 y encontramos también el tiempo de proceso al terminar el cálculo para cada valor de la energía.

CRYSTALLOGRAPHY

FE(80%) - GE(20%)

18/7/77

DISTANCE/SIDE FOR FCC, BCC AND DIAMOND

0.000000	0.705000	1.000000	1.236700	2.112000	2.581000	1.732100	1.870800
2.000000	2.121300	2.236100	2.393200	2.420500	2.495000		
2.500000	2.366050	1.000000	1.234500	1.820300	1.732100	2.000000	2.179400
2.836100	2.449500	2.594100	2.624500	2.758000	3.000000		
3.000000	2.433020	0.707100	0.629100	1.000000	1.439700	1.224700	1.299300
3.414200	1.479000	1.600700	1.639300	1.732100	1.785300		

NUMBER OF NEIGHBOUR ATOMS FOR FCC, BCC, DIAMOND AND HCP

12	6	24	12	24	8	48	6	36	24	24	24	72
8	12	12	24	6	24	24	24	36	36	12	48	50
4	12	12	2	12	24	16	12	34	34	12	48	50
6	6	6	2	12	6	12	6	12	12	6	6	12

MAXIMUM RADIUS FROM HEX = 60.00000

RECIPROCAL OF MESH INTERVAL FROM HEX = 32.00000

NUMBER OF MESH POINTS = 421

NUMBER OF TYPES OF ATOMS = 2 ATOMIC NUMBERS 26 32

TABLE OF APH RADIUS

1507331E+03	1584913E-03	1695858E-03	1751268E-03	1641956E-03	1737545E-03	2034684E-03	2139049E-03
4354626E-03	4386202E-03	4495156E-03	5018556E-03	4749556E-03	4875539E-03	5476141E-03	5713904E-03
7404514E-03	7506414E-03	5537843E-03	5314416E-03	6112683E-03	6755383E-03	4528572E-03	4761414E-03
1113775E-03	1170714E-03	1531042E-03	8674909E-03	3690350E-03	1007785E-03	1150952E-03	1150952E-03
2478752E-02	1740717E-03	1933705E-03	1739454E-02	2029456E-02	1739454E-02	1739454E-02	1739454E-02
3677864E-02	2005845E-03	1808745E-03	2079489E-02	3027555E-02	1808745E-03	1808745E-03	1808745E-03
5519505E-02	5797945E-03	1406675E-03	2093035E-02	4751555E-02	5797945E-03	5797945E-03	5797945E-03
8229747E-02	8516793E-03	9525776E-03	2090333E-02	6737394E-02	8516793E-03	8516793E-03	8516793E-03
1227734E-01	1192517E-01	1326497E-01	1429243E-01	1409538E-01	1227734E-01	1227734E-01	1227734E-01
1231564E-01	1087237E-01	1326497E-01	2127377E-01	2237377E-01	1231564E-01	1231564E-01	1231564E-01
4076220E-01	4189523E-01	1094092E-01	2173599E-01	2339737E-01	4076220E-01	4076220E-01	4076220E-01
8081449E-01	6392763E-01	1202055E-01	2352055E-01	2499375E-01	8081449E-01	8081449E-01	8081449E-01
9717179E-01	9530711E-01	1292561E-01	1063038E-01	7427353E-01	9717179E-01	9717179E-01	9717179E-01
1353535E+00	1422719E+00	1295613E+00	1295613E+00	1120203E+00	1353535E+00	1353535E+00	1353535E+00
2018965E+00	2122611E+00	2231302E+00	1327372E+00	1652930E+00	2018965E+00	2018965E+00	2018965E+00
2041230E+00	2166308E+00	2231302E+00	2493777E+00	2493777E+00	2041230E+00	2041230E+00	2041230E+00
6703240E+00	5723666E+00	2096515E+00	5723058E+00	5862937E+00	5723666E+00	5723666E+00	5723666E+00
1490840E+00	1040690E+00	7409512E+00	1040690E+00	1040690E+00	1490840E+00	1490840E+00	1490840E+00
1499084E+00	1195171E+00	1105171E+01	1105171E+01	1105171E+01	1499084E+00	1499084E+00	1499084E+00
2255555E+00	1560341E+00	1655612E+01	1655612E+01	1655612E+01	2255555E+00	2255555E+00	2255555E+00
3295611E+00	2538961E+00	2459631E+01	2459631E+01	2459631E+01	3295611E+00	3295611E+00	3295611E+00
7389555E+00	2509335E+00	2609297E+01	2609297E+01	2609297E+01	7389555E+00	7389555E+00	7389555E+00
1642316E+00	2767670E+00	5673947E+01	8166170E+01	8580158E+01	1642316E+00	1642316E+00	1642316E+00
4553285E+00	1128087E+00	1618124E+01	1618124E+01	1618124E+01	4553285E+00	4553285E+00	4553285E+00
36559823E+00	2579403E+00	18171264E+02	1915945E+02	2008053E+02	36559823E+00	36559823E+00	36559823E+00
	3847467E+02	27711264E+02	2850273E+02	2890641E+02		3311545E+02	3813132E+02

INTERPOLATED TABLE OF 4*PI*(R**2)*ARHO FOR THIS PROGRAM, FOR THE 1 ATOM

4178490E+02	4497670E-02	5080883E-02	5093582E-02	6177696E-02	6811937E-02	7510880E+02	828805E-02
4497684E+01	2144530E-01	2148651E-01	2265531E-01	3079620E-01	1480633E-01	1630816E-01	1806425E-01
4329963E+01	4177290E-01	5255031E-01	5780618E-01	6375949E-01	7235968E-01	3566809E-01	3733022E-01
937566E+01	1033350E+00	1134474E+00	1250932E+00	1370932E+00	1513427E+00	7733375E-01	8515816E-01
2017741E+00	2219298E+00	2446612E+00	2604556E+00	2842957E+00	3053658E+00	1834227E+00	1915558E+00
4301317E+00	4720058E+00	5187172E+00	5694315E+00	6248034E+00	6855925E+00	1824780E+00	1945801E+00
9041579E+00	9058582E+00	1085520E+00	1180222E+00	1252132E+00	1352138E+00	1557681E+00	1623140E+00
14861244E+01	2335094E+01	2219697E+01	2321212E+01	2420473E+01	2504056E+01	1577681E+01	1623140E+01
7713449E+01	4137120E+01	4345304E+01	4759721E+01	5161719E+01	5592067E+01	3139215E+01	3413902E+01
1257845E+02	7353009E+01	8230957E+01	8062210E+01	9131618E+01	1026277E+01	6057458E+01	654779E+01
1341555E+02	1313717E+02	1525541E+02	1643245E+02	1763684E+02	1422625E+02	1878172E+02	1916128E+02
2290179E+02	2228192E+02	2225967E+02	2320324E+02	2420326E+02	2520327E+02	1815501E+02	1916128E+02
2807200E+02	2872006E+02	2941613E+02	3002326E+02	3053213E+02	3093710E+02	2621159E+02	2710758E+02
3344515E+02	3315801E+02	3118822E+02	3083072E+02	3053213E+02	3093710E+02	322793E+02	3340033E+02
2249312E+02	2733009E+02	2664176E+02	2599573E+02	2542059E+02	2494176E+02	2498857E+02	2471929E+02
2436284E+02	2451257E+02	2485075E+02	2537170E+02	2600717E+02	2624947E+02	2624947E+02	2439470E+02
3440764E+02	3124614E+02	3233095E+02	3252573E+02	3200534E+02	3453260E+02	3454702E+02	2999866E+02
2149362E+02	3309610E+02	3477327E+02	3144710E+02	3591304E+02	2840641E+02	2612029E+02	3484868E+02
1227140E+02	1504517E+02	1617074E+02	1645759E+02	1519251E+02	1480641E+02	1433208E+02	2396148E+02
1671485E+02	1531477E+02	1354230E+02	1415346E+02	1413842E+02	1492500E+02	1499560E+02	1303161E+02
4179837E+02	1026211E+02	1063594E+02	1020222E+02	1060977E+02	1049250E+02	1049956E+02	1044120E+02
2255274E+01	3364203E+01	3352021E+01	3541794E+01	3750653E+01	653380E+01	5651412E+01	5996807E+01
4659428E+01	4193200E+01	4035020E+01	4013788E+01	2239123E+01	1925746E+01	1882844E+01	1441239E+01
1540644E+00	1326203E+00	1405050E+00	14171079E+00	2774412E+00	2419938E+00	2092973E+00	1624268E+00
4191693E+00	3165203E+00	1428655E+00	1467658E+00	2629058E+00	2824170E+00	209356E+00	1916086E+00
1497357E+01	1617106E+01	1467658E+01	2583597E+01	2284049E+01	7037356E+01	8921469E+01	9140508E+01
3722222E+01	2025035E+02	1161340E+01	1004921E+01	8624207E+02	2034316E+01	8931773E+01	17430508E+01
1686717E+03	65991407E+02	2074920E+02	1489008E+02	1033315E+02	694703E+02	4497214E+02	2837419E+02
5333836E-06	2031401E-06	3363035E-04	2825233E-04	1419428E-04	6797598E-05	3363489E-05	1322243E-05

INTERPOLATED TABLE OF 4*PI*(R**2)*RHO FOR THIS PROGRAM, FOR THE 2 ATOM

8696752E-02	2580113E-02	1055294E-01	1162423E-01	1280393E-01	1410273E-01	1553322E-01	1718047E-01
1884186E-01	2075003E-01	1185119E-01	1161640E-01	1271123E-01	1305133E-01	1355332E-01	1468947E-01
4072629E-01	1448350E-01	4935412E-01	5116120E-01	5790212E-01	6582124E-01	7244249E-01	797113E-01
8772296E-01	2652398E-01	1091195E-00	1140205E-00	1245115E+00	1413208E+00	1554568E+00	1703513E+00
1877923E+00	2062637E+00	1091175E+00	1140205E+00	1244114E+00	1413208E+00	1554568E+00	1703513E+00
1996842E+00	2380467E+00	1081268E+00	1152338E+00	1284211E+00	1413208E+00	1531275E+00	1638973E+00
8399662E+00	1929727E+00	1081268E+00	1152338E+00	1284211E+00	1413208E+00	1531275E+00	1638973E+00
1735202E+01	1802108E+01	1081268E+00	1152338E+00	1284211E+00	1413208E+00	1531275E+00	1638973E+00
4433422E+01	1803697E+01	413693AE+01	425880AE+01	1210414E+01	1325105E+01	1450316E+01	1586672E+01
6768679E+01	1803697E+01	413693AE+01	425880AE+01	1210414E+01	1325105E+01	1450316E+01	1586672E+01
1238766E+02	1328106E+02	7322047E+01	8552197E+01	9237112E+01	2211123E+01	2941617E+01	32626572E+01
2083326E+02	1220597E+02	1423787E+02	1523176E+02	1733237E+02	1972172E+02	1953177E+02	1963698E+02
3094468E+02	1341975E+02	2331117E+02	2715240E+02	2715240E+02	2715240E+02	2715240E+02	2977283E+02
3847641E+02	3489726E+02	3830515E+02	3830515E+02	3830515E+02	3830515E+02	3830515E+02	3791433E+02
3819651E+02	3212011E+02	3828287E+02	3825599E+02	3824809E+02	3824809E+02	3824809E+02	3807144E+02
3220342E+02	3757424E+02	3686841E+02	3686841E+02	3686841E+02	3686841E+02	3686841E+02	33096687E+02
3497925E+02	3212011E+02	3212011E+02	3196123E+02	3196123E+02	3196123E+02	3196123E+02	33096687E+02
4551294E+02	3692197E+02	3760131E+02	3760131E+02	3760131E+02	3760131E+02	3760131E+02	33096687E+02
3825747E+02	4362125E+02	4576116E+02	4576116E+02	4576116E+02	4576116E+02	4576116E+02	4431376E+02
27741489E+02	3597157E+02	3391195E+02	3120308E+02	29707114E+02	2760873E+02	2662114E+02	4035504E+02
27741489E+02	2279102E+02	2276451E+02	2319869E+02	2375114E+02	2400845E+02	2411012E+02	2411012E+02
64411626E+02	2297091E+02	2064204E+02	2051972E+02	2051972E+02	2051972E+02	2051972E+02	2059442E+02
2874202E+01	16233577E+01	6039556E+01	6011316E+01	1916454E+01	1954455E+01	1954455E+01	20587823E+02
2874202E+01	2603262E+01	2388111L+01	2210619E+01	2080595E+01	1963208E+01	1963208E+01	1967834E+01
45530261E+01	1586229E+01	1491148E+01	1498354E+01	1425742E+01	1483308E+01	1483308E+01	1475568E+01
2753395E+00	1586229E+00	1491148E+00	1498354E+00	1523430E+00	1531087E+00	1531087E+00	1523430E+00
3809486E+00	2257209E+00	1857528E+00	1487678E+00	1175294E+00	9124755E+00	6955517E+00	3200032E+00
209847E+00	725712E+01	153021E+01	153021E+01	1671492E+01	5609428E+01	3528627E+02	2123067E+02
4733072E+00	192549E+00	798564E+00	798564E+00	2124476E+00	4094278E+00	2048357E+00	1987014E+00
4987178E+00	1103732E+00	350205E+00	350205E+00	203778E+00	4094278E+00	3040117E+00	2070552E+00
1550440E+15	1261041E+16	2025227E+10	3524948E+11	5799778E+12	8700334E+13	1109433E+13	14774428E+14

INTEGRAL OF CHARGE DENSITY FOR THE 1 ATOM

25.93825116

INTEGRAL OF CHARGE DENSITY FOR THE 2 ATOM

31.99813193

LATTICE STRUCTURE:
HIGH POINT CORRESPONDING TO THE APW SPHERE RADIUS=194.850000
VOLUME PER ATOM(ATOMIC UNITS)= 87.740900
LATTICE CONSTANTS A AND C 7.053770 7.053770
EXCHANGE COEFFICIENTS ALPHA AND BETA 0.003000 0.003000

NEIGHBOR DISTANCES AND NUMBER OF NEIGHBORS ---CENTRAL ATOM OF TYPE--- 1
 8.899881 4.972901 6.353750 8.938749 9.975427 11.152700 12.217818 7.053760
 7.053760

1.0000000 2.0000000 3.0000000 19.0000000 10.0000000 19.0000000 6.0000000 0.0000000

NEIGHBOR DISTANCES AND NUMBER OF NEIGHBORS ---CENTRAL ATOM OF TYPE--- 2
 8.892890 7.97291 6.53760 6.038740 9.9738470 9.975427 11.152700 12.215818 7.053760
 7.053760

10.000000 5.000000 1.000000 5.000000 2.000000 5.000000 2.000000 0.000000

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INTEGRAL OF POTENTIAL IN THE MUFFIN TIN SPHERE= -606796E-01
INTEGRAL OF 4*PI*T**HUE= 123986E+00
CHARGE INTO THE SPHERE= .254699E+02
VOLUME= 69414E+02
EXCHANGE POTENTIAL= 248549E+00
NUMBER OF ATOMS OF TYPE 1= .660000E+02
NUMBER OF ATOMS OF TYPE 2= .170000E+02

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INTEGRAL OF POTENTIAL IN THE HUFFIN TIN SPHERE= -.720954E-01
INTEGRAL OF POTENTIAL = 1400000E+00
CHARGE INTO THE SPHERE= .3057E+02
EXCHANGE POTENTIAL= .999411E+02
NUMBER OF ATOMS OF TYPE 1= 967617E+00
NUMBER OF ATOMS OF TYPE 2= .170000E+02
NUMBER OF ATOMS OF TYPE 3= .660000E+02

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CRYSTALLOGRAPHIC DATA

FE(80%) - GE(20%) 18/7/77

CENTRAL ATOM OF TYPE 2

RESULTS FOR MUFFIN TIN WITH RI(1)= 2.4412 RI(2)= 2.4412 RO= 2.7566 V BOUNDARY= -.6004950E+00
 VINT= -1.4884643E+01 Z= 32.00 JRI(1)=194.850000 JRI(2)=194.850000 LAT= 6
 XALPHA= 0.6666667 XRETA= 0.0030000

= 42439722E+06	= 40368951E+06	= 38399171E+06	= 36525459E+06	= 34743127E+06
= 324947721E+06	= 31434990E+06	= 29900932E+06	= 28441678E+06	= 27053595E+06
= 26533246E+06	= 2457213E+06	= 23292479E+06	= 2149004E+06	= 21064959E+06
= 20036639E+06	= 195317E+06	= 18121997E+06	= 1724239E+06	= 1641198E+06
= 14214493E+06	= 143317E+06	= 14101664E+06	= 134293352E+06	= 12768656E+06
= 94259979E+06	= 931636E+06	= 10250726E+06	= 1045942E+06	= 9939754E+06
= 73581778E+06	= 691163E+06	= 92564703E+06	= 91349251E+06	= 7736427E+06
= 57266618E+06	= 599123E+06	= 806264703E+06	= 8054021E+06	= 60243775E+06
= 44531969E+06	= 54453037E+06	= 7078209E+06	= 70540352E+06	= 46835562E+06
= 34032933E+06	= 52756037E+06	= 6172782E+06	= 6172782E+06	= 36421401E+06
= 26915634E+06	= 5231520E+06	= 513130E+06	= 513130E+06	= 28368682E+06
= 20914220E+06	= 25530150E+05	= 4086804E+06	= 4086804E+06	= 21989490E+06
= 16222074E+06	= 19871064E+05	= 3145864E+06	= 3145864E+06	= 17067313E+06
= 12523398E+06	= 19130067E+05	= 2145232E+06	= 2145232E+06	= 153233811E+06
= 97351683E+06	= 19494068E+05	= 12135232E+06	= 12135232E+06	= 124247811E+06
= 75233679E+06	= 21474925E+04	= 10728067E+06	= 10728067E+06	= 10226729E+06
= 58014945E+04	= 71437393E+04	= 9078356E+04	= 9078356E+04	= 61222729E+04
= 44613207E+04	= 6505467E+04	= 5224782E+04	= 5224782E+04	= 5103135E+04
= 34189906E+04	= 52315362E+04	= 4012674E+04	= 4012674E+04	= 398104E+04
= 26091928E+04	= 32402478E+04	= 30723072E+04	= 30723072E+04	= 260511485E+04
= 19301983E+04	= 24794109E+04	= 23385672E+04	= 23385672E+04	= 205111485E+04
= 14921528E+04	= 18734653E+04	= 177131313E+04	= 177131313E+04	= 15621887E+04
= 11185793E+04	= 14113693E+04	= 133233131E+04	= 133233131E+04	= 118621839E+04
= 82907705E+03	= 1054126E+04	= 923520521E+03	= 923520521E+03	= 804050521E+03
= 62041809E+03	= 77919128E+03	= 7333311E+03	= 689336679E+03	= 64775150E+03
= 4417651E+03	= 5712122E+03	= 5361060E+03	= 502807799E+03	= 47147459E+03
= 31587354E+03	= 413600431E+03	= 38709164E+03	= 361970978E+03	= 33623211E+03
= 2214747945E+03	= 29465402E+03	= 27469591E+03	= 25683388E+03	= 238129E+03
= 15181298E+03	= 20578178E+03	= 19101597E+03	= 177131778E+03	= 16413179E+03
= 1308587E+03	= 1402056E+03	= 12945625E+03	= 119220597E+03	= 10947454E+03
= 6556884E+02	= 92561974E+02	= 8486364E+02	= 777441360E+02	= 71158731E+03
= 40196659E+02	= 59418678E+02	= 54166021E+02	= 492730013E+02	= 44124310E+02
= 2304280E+02	= 36579609E+02	= 32962907E+02	= 27939043E+02	= 26586803E+02
= 13346281E+02	= 21270536E+02	= 18974575E+02	= 168392565E+02	= 15194342E+02
= 71159342E+01	= 11335362E+02	= 10480033E+02	= 92645599E+01	= 8194342E+01
= 36111404E+01	= 63171372E+01	= 55275506E+01	= 48170626E+01	= 41805474E+01
= 19209149E+01	= 31047117E+01	= 26596068E+01	= 22726640E+01	= 18379749E+01
= 67341671E+00	= 40031054E+01	= 18766295E+01	= 20800308E+01	= 16285126E+00
= 16407426E+00	= 54145024E+00	= 42195474E+00	= 31806473E+00	= 23726565E+00
= 11297630E+00	= 11522045E+00	= 8996618E+00	= 80805858E+00	= 9792435E+00
= 19206673E+01	= 22537677E+00	= 57319589E+00	= 63498804E+00	= 10717987E+01
= 112650511E+01	= 21007610E+01	= 4228290E+01	= 5586671E+01	= 43082022E+01
= 22026610E+01	= 11666910E+01	= 57113053E+00	= 50937754E+00	= 14313742E+01
= 22033121E+01	= 1093342E+01	= 65134658E+00	= 21106473E+01	= 426471330E+01
= 49712802E+00	= 11520228E+01	= 21179732E+01	= 11849535E+01	= 21447016E+01
0.	= 61157107E+00	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.

CRYSTALLOGRAPHY

FE(80%) - GE(20%)

18/7/77

R*V(R)	63970473E+02	63963938E+02	63967323E+02	63965624E+02	6396337E+02
63961956E+02	6395977E+02	63957095E+02	63955705E+02	63955705E+02	63953400E+02
63950916E+02	63944245E+02	63945740E+02	63942915E+02	63942915E+02	63939443E+02
63936816E+02	63933525E+02	63930836E+02	63929415E+02	63929415E+02	63922500E+02
63931859E+02	63931303E+02	63930834E+02	63929130E+02	63929130E+02	639201178E+02
63930490E+02	63930471E+02	63930834E+02	63928750E+02	63928750E+02	63871145E+02
63864348E+02	63865716E+02	63864956E+02	63863152E+02	63863152E+02	63832991E+02
63823912E+02	63814327E+02	63814102E+02	63813295E+02	63813295E+02	63781655E+02
63763347E+02	63766208E+02	63742952E+02	63729295E+02	63729295E+02	63711577E+02
63709477E+02	63707087E+02	63657525E+02	63637729E+02	63637729E+02	63610483E+02
63599380E+02	63599344E+02	63544670E+02	63533794E+02	63533794E+02	63489666E+02
63505981E+02	63429313E+02	63395139E+02	63395050E+02	63395050E+02	63323228E+02
63261306E+02	63245336E+02	63245336E+02	63245336E+02	63245336E+02	63187993E+02
63156833E+02	63153871E+02	63153871E+02	63153871E+02	63153871E+02	62620118E+02
62716339E+02	62705261E+02	62623236E+02	62624095E+02	62624095E+02	62467920E+02
62286414E+02	62290085E+02	62207443E+02	62209071E+02	62209071E+02	62010394E+02
61190392E+02	61172577E+02	61167574E+02	61153124E+02	61153124E+02	61426038E+02
61080806E+02	6111405614E+02	61080568E+02	6095585611E+02	6095585611E+02	6095585611E+02
60913139E+02	60933523E+02	6091500145E+02	6091500145E+02	6091500145E+02	609253415E+02
597941107E+02	597941107E+02	597089193E+02	597089193E+02	597089193E+02	585097718E+02
59531309E+02	595064197E+02	59780820E+02	59780820E+02	59780820E+02	58545226E+02
595681616E+02	595291804E+02	59184220E+02	59184220E+02	59184220E+02	59184220E+02
592904221E+02	592422005E+02	59242505E+02	59318147E+02	59318147E+02	59336968E+02
54951229E+02	54951454E+02	54922667E+02	549494046E+02	549494046E+02	54987394E+02
44136009E+02	44138242E+02	44138242E+02	44519743E+02	44519743E+02	4410232164E+02
44116160E+02	44143105E+02	44272605E+02	44199051E+02	44199051E+02	441236424E+02
36561626E+02	36561626E+02	36870736E+02	36849571E+02	36849571E+02	37213157E+02
34790155E+02	34790155E+02	34623553E+02	34623553E+02	34623553E+02	328206157E+02
25441614E+02	250964927E+02	250017441E+02	25049648E+02	25049648E+02	250669518E+02
25552740E+02	25121375E+02	251120212E+02	25144717E+02	25144717E+02	25149217E+02
17280727E+02	16521588E+02	16362978E+02	16494325E+02	16494325E+02	163774303E+02
17044489E+02	16190101E+02	161149636E+02	160330192E+02	160330192E+02	16541809E+02
545291135E+01	54809723E+01	548269729E+01	548361674E+01	548361674E+01	54949308E+01
55556126E+01	521753113E+01	542461747E+01	536795541E+01	536795541E+01	531277539E+01
-16342592E+01	-17050447E+01	-15807077E+01	-14120323E+01	-14120323E+01	-1675919E+01
-14045033E+01	-24948298E+01	-23151360E+01	-20936053E+01	-20936053E+01	-12641842E+01
-14045033E+01	-34726527E+01	-34006229E+01	-27369716E+01	-27369716E+01	-30897491E+01
-63607782E+00	-47156360E+01	-40926591E+01	-1243644E+01	-1243644E+01	-43915934E+01
-22984431E+01	-21957975E+01	-16306636E+02	-25550573E+02	-25550573E+02	-16896623E+02
-65821602E+01	-50657559E+01	-37308080E+01	-74987790E+01	-74987790E+01	-14682767E+02
-69930118E+01	-31863754E+01	-986895125E+01	-318024836E+01	-318024836E+01	-38169844E+01
			-72348115E+01	-72348115E+01	

CRYSTAL/DERIV/ASIL FE(80%) - GE(20%)

18/7/77

ADDITIONAL VINT FOR DERILOG= 0.0000
 LMAX= 2
 NUMBER OF ENERGIES= 60
 BOTTOM ENERGY= 0.0000
 STEP ENERGY= 0.0200

LOGARITHMIC DERIVATIVES FOR L=0 TO L=2

ENERGY	L=0	L=1	L=2
0.0100	-7447266E+00	-1001880E-01	-7201751E+00
0.0300	-77557324E+00	-1001880E-02	-7100542E+00
0.0500	-7171328E+00	-7255839E-01	-7073232E+00
0.0700	-87914638E+00	-7255839E-01	-6973232E+00
0.0900	-87272085E+00	-4178900E-01	-6833360E+00
0.1100	-9067947E+00	-5665461E-01	-6740941E+00
0.1300	-94179375E+00	-7167900E-01	-6646607E+00
0.1500	-9777695L+00	-8697921E-01	-6556697E+00
0.1700	-1014730L+01	-10230256E+00	-6497297E+00
0.1900	-1052736E+01	-11702251E+00	-6397297E+00
0.2100	-1091892L+01	-13306396E+00	-6278831E+00
0.2300	-132192L+01	-14920407E+00	-618048E+00
0.2500	-173719L+01	-16531355E+00	-6073191E+00
0.2700	-214530L+01	-1821924E+00	-5995071E+00
0.2900	-260714L+01	-1987824E+00	-5906644E+00
0.3100	-316326L+01	-2155892E+00	-5811155E+00
0.3300	-3753453L+01	-2329112E+00	-5716337E+00
0.3500	-4402180L+01	-24927155E+00	-5625326E+00
0.3700	-5152691L+01	-2673470E+00	-5531057E+00
0.3900	-5904816L+01	-2657390E+00	-5430520E+00
0.4100	-675933L+01	-3031762E+00	-5341697E+00
0.4300	-6150692L+01	-3213112E+00	-5265575E+00
0.4500	-6737352L+01	-3390051E+00	-5151142E+00
0.4700	-733921L+01	-3583672E+00	-5055385E+00
0.4900	-796924L+01	-3776951E+00	-4959291E+00
0.5100	-862527L+01	-3967066E+00	-4862841E+00
0.5300	-930920E+01	-4165600E+00	-4766043E+00
0.5500	-2012295L+01	-4361338E+00	-4660833E+00
0.5700	-2070810E+01	-4566769E+00	-4571299E+00
0.5900	-2154781L+01	-4772194E+00	-4473335E+00
0.6100	-2236437E+01	-4983779E+00	-4374962E+00
0.6300	-2322000E+01	-5192956E+00	-4276137E+00
0.6500	-2411939E+01	-5409517E+00	-4176932E+00
0.6700	-2500556L+01	-5627973E+00	-4077265E+00
0.6900	-2600160L+01	-5851535E+00	-3977134E+00
0.7100	-2711241E+01	-6077232E+00	-3876532E+00
0.7300	-2822291L+01	-6307358E+00	-3775455E+00
0.7500	-293861L+01	-6542572E+00	-367380E+00
0.7700	-3054578L+01	-6781198E+00	-357180E+00
0.7900	-3171138L+01	-7026777E+00	-3464218E+00
0.8100	-3290150L+01	-7552057E+00	-3366190E+00
0.8300	-3401250L+01	-7552057E+00	-3262133E+00
0.8500	-3505518L+01	-7782241E+00	-3158235E+00
0.8700	-3625726L+01	-8040476E+00	-3053406E+00
0.8900	-4010151L+01	-8511873E+00	-2970114E+00
0.9100	-4211419L+01	-8584619E+00	-2842185E+00

0.9300	-4429436E+01	-8862907E+00	2735652E+00
0.9500	-4666451E+01	-9156941E+00	2620852E+00
0.9700	-4792912E+01	-9729974E+00	2411432E+00
0.9900	-5220816E+01	-9735172E+00	2310427E+00
1.0100	-5320911E+01	-1033557E+01	2309427E+00
1.0300	-5388569E+01	-1037505E+01	2308356E+00
1.0500	-6271629E+01	-1093473E+01	2083167E+00
1.0700	-6676297E+01	-1115701E+01	1972070E+00
1.0900	-7182222E+01	-1155410E+01	1747730E+00
1.1100	-8358639E+01	-1201143E+01	1634530E+00
1.1300	-9310420E+01	-1231607E+01	1620571E+00
1.1500	-29985274E+01	-1272117E+01	1705832E+00
1.1700	-1079851E+02	-1307172E+01	1290320E+00

PHASE SHIFTS

ENERGY	L=0	L=1	L=2
0.6100	-534144E+00	.2241289E-02	.9155811E-06
0.6300	-560124E+00	.160150E-01	.4696240E-04
0.6500	-1056295E+01	.2673324E-01	.530339E-04
0.6700	-1177612E+01	.4374416E-01	.1238139E-03
0.6900	-1317221E+01	.633105E-01	.2333334E-03
0.7100	-1377971E+01	.828562E-01	.347765E-03
0.7300	-1475677E+01	.1115739E+00	.5993809E-03
0.7500	-1513825E+01	.1503770E+00	.8093504E-03
0.7700	-1530922E+01	.1679756E+00	.11626302E-03
0.7900	-1618351E+01	.1945507E+00	.1536082E-03
0.8100	-1431421E+01	.2303195E+00	.1880997E-03
0.8300	-1314851E+01	.2639542E+00	.2491331E-03
0.8500	-1314153E+01	.2751408E+00	.3073032E-03
0.8700	-1310973E+01	.3275926E+00	.3728905E-03
0.8900	-1262805E+01	.3629880E+00	.4461331E-02
0.9100	-1220716E+01	.3995570E+00	.5272581E-02
0.9300	-1122461E+01	.4251512E+00	.6164798E-02
0.9500	-1159352E+01	.4621533E+00	.7139852E-02
0.9700	-1120667E+01	.4900858E+00	.8199452E-02
0.9900	-1190811E+01	.5213937E+00	.9345129E-02
0.4100	-1073144E+01	.5490140E+00	.1575825E-01
0.4300	-1042550E+01	.5751549E+00	.1190001E-01
0.4500	-1015963E+01	.6005457E+00	.1331145E-01
0.4700	-9902776E+00	.6247780E+00	.1481347E-01
0.4900	-9654306E+00	.64721293E+00	.1640679E-01
0.5100	-9411369E+00	.6681754E+00	.1709262E-01
0.5300	-9181114E+00	.6873899E+00	.1986330E-01
0.5500	-8955347E+00	.7057679E+00	.2173934E-01
0.5700	-8732861E+00	.7224893E+00	.2370227E-01
0.5900	-8513250L+00	.7473927E+00	.2575459E-01
0.6100	-8301186L+00	.7523384E+00	.2794894E-01
0.6300	-8105316E+00	.7649875E+00	.30104827E-01
0.6500	-7906356L+00	.7768926E+00	.3208823E-01
0.6700	-7712037L+00	.7875409E+00	.3490778E-01
0.6900	-7522115L+00	.7972775E+00	.3742436E-01
0.7100	-7333394E+00	.8069622E+00	.4042263E-01
0.7300	-7145578L+00	.8137551E+00	.4355235E-01
0.7500	-6976567L+00	.8221012E+00	.4655328E-01
0.7700	-6832134L+00	.83272844E+00	.4930664E-01
0.7900	-6631765L+00	.8432952E+00	.5245968E-01
0.8100	-64123483E+00	.8540035E+00	.55735195E-01
0.8300	-6228735E+00	.8645002E+00	.5867106E-01
0.8500	-6137499E+00	.8745199E+00	.61453264E-01
0.8700	-6028759E+00	.8843379E+00	.64359276E-01
0.8900	-5922639E+00	.89511179E+00	.67359423E-01
0.9100	-5856973E+00	.9059187E+00	.7056623E-01
0.9300	-5751940E+00	.92547718E+00	.74362638E-01
0.9500	-5652191E+00	.9457792E+00	.7796408E-01
0.9700	-5535137E+00	.9667207E+00	.81693337E-01
0.9900	-5406110L+00	.98714042E+00	.8537214E-01
1.0100	-5301370E+00	.10072411E+00	.89178119E-01
1.0300	-5209439E+00	.10267920E+00	.9304928E-01
1.0500	-5129411E+00	.10459364E+00	.9698307E-01
1.0700	-5052911E+00	.10555000E+00	.1009772E+00
1.0900	-4979311E+00	.1054613E+00	.1050291E+00
1.1100	-4826224L+00	.10531176E+00	.1081301E+00
1.1300	-47135943E+00	.10515450E+00	.1132664E+00

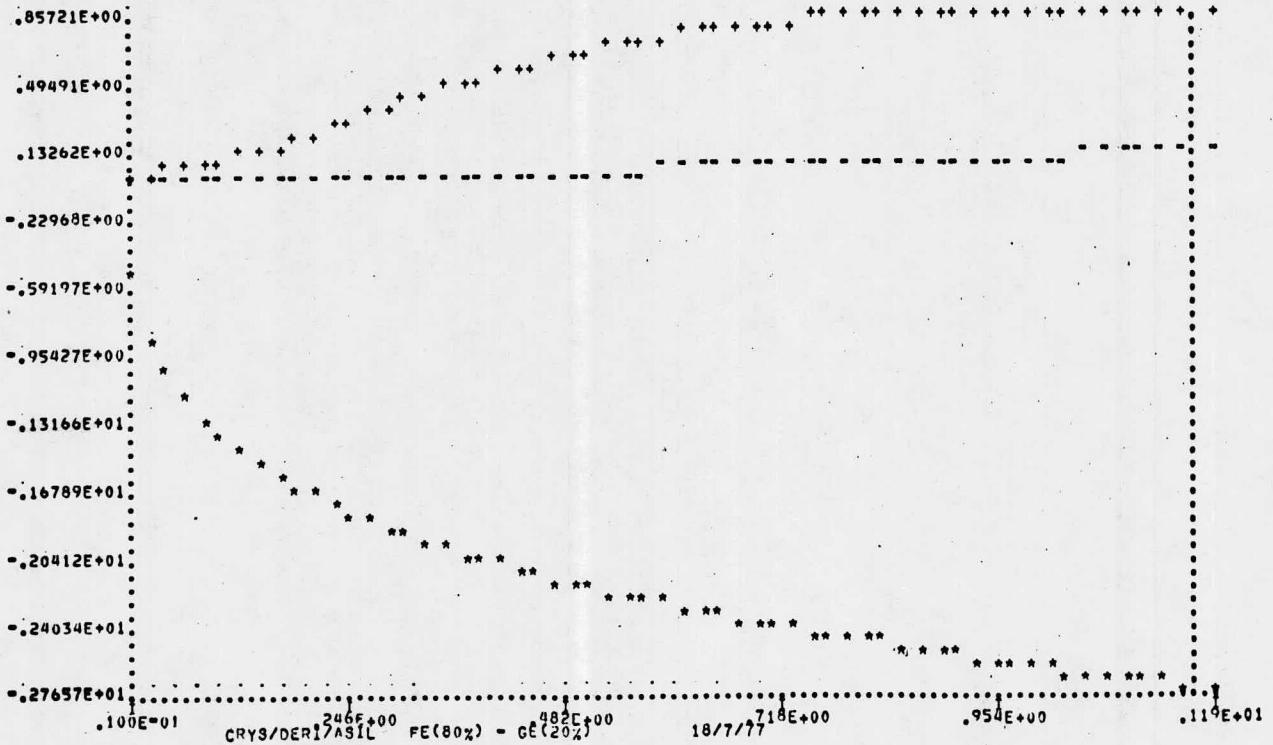
1.1500 .4008424E+00 .8497585E+00 .1175066E+00
 1.1700 .3082636L+00 .8477722E+00 .1217647L+00
 1.1900 .3750530L+00 .8455990E+00 .1260666E+00

CEP***

0.0100	.2323065E+01	.6596985E+03	.1121542E+07
0.0300	.15635597L+01	.6052846E+03	.1425407E+05
0.0500	.10355597L+01	.6052846E+03	.1425407E+05
0.0700	.2351944E+00	.3701395E+02	.A5125596E+04
0.0900	.8422592E+00	.2573670E+02	.45208891E+04
0.1100	.7741447L+00	.1926605E+02	.27357193E+04
0.1300	.73097380E+00	.1510696E+02	.1737947E+04
0.1500	.67498441E+00	.1243749E+02	.9254874E+03
0.1700	.6067785L+00	.941389E+02	.9257600E+03
0.1900	.6472152E+00	.8271636E+01	.6432552E+03
0.2100	.6257158E+00	.7777479E+01	.5101230E+03
0.2300	.6190347E+00	.6870701E+01	.4305201E+03
0.2500	.5900001E+00	.6133061E+01	.3405201E+03
0.2700	.58041197E+00	.5530163E+01	.2942939E+03
0.2900	.5370239E+00	.5037274E+01	.2942939E+03
0.3100	.5731291E+00	.4014496E+01	.2052296E+03
0.3300	.5075134E+00	.4253306E+01	.1759912E+03
0.3500	.5030232E+00	.3942516E+01	.1329478E+03
0.3700	.5572153E+00	.3072030E+01	.1329478E+03
0.3900	.2369750E+00	.3435093E+01	.1169273E+03
0.4100	.2512794E+00	.3223933E+01	.1135443E+03
0.4300	.2512794E+00	.3042430E+01	.9226420E+02
0.4500	.2512794E+00	.2074350E+01	.8267932E+02
0.4700	.2512794E+00	.2725384E+01	.7447478E+02
0.4900	.2512794E+00	.2521144E+01	.67442287E+02
0.5100	.2512794E+00	.24250716E+01	.6292210E+02
0.5300	.2512794E+00	.20239192E+01	.5922103E+02
0.5500	.2512794E+00	.20239192E+01	.5922103E+02
0.5700	.2512794E+00	.20239192E+01	.5922103E+02
0.5900	.2512794E+00	.20239192E+01	.5922103E+02
0.6100	.2512794E+00	.20239192E+01	.5922103E+02
0.6300	.2512794E+00	.20239192E+01	.5922103E+02
0.6500	.2512794E+00	.20239192E+01	.5922103E+02
0.6700	.2512794E+00	.20239192E+01	.5922103E+02
0.6900	.2512794E+00	.20239192E+01	.5922103E+02
0.7100	.2512794E+00	.20239192E+01	.5922103E+02
0.7300	.2512794E+00	.20239192E+01	.5922103E+02
0.7500	.2512794E+00	.20239192E+01	.5922103E+02
0.7700	.2512794E+00	.20239192E+01	.5922103E+02
0.7900	.2512794E+00	.20239192E+01	.5922103E+02
0.8100	.2512794E+00	.20239192E+01	.5922103E+02
0.8300	.2512794E+00	.20239192E+01	.5922103E+02
0.8500	.2512794E+00	.20239192E+01	.5922103E+02
0.8700	.2512794E+00	.20239192E+01	.5922103E+02
0.8900	.2512794E+00	.20239192E+01	.5922103E+02
0.9100	.2512794E+00	.20239192E+01	.5922103E+02
0.9300	.2512794E+00	.20239192E+01	.5922103E+02
0.9500	.2512794E+00	.20239192E+01	.5922103E+02
0.9700	.2512794E+00	.20239192E+01	.5922103E+02
0.9900	.2512794E+00	.20239192E+01	.5922103E+02
1.0100	.2512794E+00	.170303E+01	.5044301E+02
1.0300	.2512794E+00	.154208E+01	.2551552E+02
1.0500	.2512794E+00	.132970E+01	.1155640E+02
1.0700	.2512794E+00	.112693E+01	.1112055E+02
1.0900	.2512794E+00	.103154E+01	.1112055E+02

1.1100	.6379972L+00	.1074415E+01	.1071074E+02
1.1300	.6345681L+00	.1050375E+01	.1032494E+02
1.1500	.6279147L+00	.1030468E+01	.9961325E+01
1.1700	.6187014L+00	.1022325L+01	.9618248E+01
1.1900	.6064037L+00	.1000170L+01	.9284184E+01

FERMI LEVEL= 1.16916 RYDBERGS
VALEUCE= 4.000000
FOR L = 0 PHASESHIFT AT FERMI LEVEL= -2.75280175
FOR L = 1 PHASESHIFT AT FERMI LEVEL= 0.84785990
FOR L = 2 PHASESHIFT AT FERMI LEVEL= 0.12158353



CRYSTAL DERI/ASIL FE(80%) - GE(20%)

18/7/77

CENTRAL ATOM OF TYPE 1

RESULTS FOR MUFFIN TIN WITH R1(1) = 2.4412 RI(2) = 2.4412 RO = 2.7566 V BOUNDARY = .1050246E+01
 VINT = -1438658E+01 Z = 26.00 JRI(1) = 194.850000 JRI(2) = 194.850000 XALPHA = 0.6660667 XBETA = 0.0030000 LAT = 6

34484092E+06	-32001594E+06	-31201152E+06	-29678764E+06	-28308364E+06
-26853149E+06	-25347777E+06	-24618594E+06	-23195494E+06	-24171556E+06
-29910045E+06	-19349545E+06	-18469545E+06	-17495494E+06	-17426456E+06
-18291842E+06	-15426812E+06	-14730281E+06	-14019175E+06	-14126456E+06
-12090625E+06	-12426032E+06	-11469256E+06	-10491912E+06	-10476456E+06
-62696735E+05	-93279274E+05	-84296044E+05	-84929037E+05	-84779445E+05
-76332160E+05	-73379397E+05	-69507680E+05	-66113889E+05	-62879161E+05
-59903267E+05	-56291256E+05	-54099773E+05	-51415388E+05	-48936961E+05
-46534271E+05	-42429311E+05	-42099511E+05	-40037485E+05	-3907662E+05
-38261717E+05	-34743510E+05	-32749707E+05	-31141109E+05	-29616739E+05
-14093095E+05	-26011421E+05	-19466620E+05	-24215733E+05	-2402301E+05
-12001859E+05	-19011020E+05	-15377299E+05	-14138977E+05	-17881424E+05
-12524179E+05	-12231616E+05	-11200295E+05	-11133873E+05	-13891845E+05
-92532842E+04	-75509173E+04	-12400472E+04	-87079426E+04	-8777462E+04
-67355740E+04	-50459567E+04	-55046564E+04	-80112957E+04	-83499520E+04
-37981578E+04	-34508933E+04	-35536255E+04	-52508191E+04	-64601233E+04
-26587612E+04	-26535250E+04	-36266255E+04	-4049422E+04	-49881393E+04
-19269547E+04	-15301252E+04	-36112106E+04	-51113333E+04	-38420536E+04
-92537184E+03	-97135762E+03	-36526200E+04	-28262683E+04	-29529916E+04
-88710576E+03	-84037274E+03	-32164028E+03	-18162007E+04	-22576394E+04
-50555988E+03	-47181476E+03	-32164028E+03	-19369532E+04	-17191764E+04
-36798353E+03	-34193499E+03	-34578685E+03	-51735180E+03	-54819353E+03
-26487954E+03	-24755226E+03	-35216320E+03	-50291185E+03	-539241475E+03
-18745554E+03	-17515522E+03	-36252645E+03	-50291185E+03	-56832164E+03
-83001824E+03	-12452405E+03	-31765842E+03	-41056186E+03	-42011183E+03
-88101824E+03	-81220477E+03	-38000159E+03	-40284945E+03	-49520148E+03
-57660190E+02	-52009787E+03	-48000159E+03	-43362820E+03	-46993377E+03
-36461143E+02	-33218285E+03	-32246270E+03	-27040850E+03	-24881690E+03
-22419429E+02	-21157217E+03	-21062167E+03	-16129979E+03	-17572967E+03
-12717657E+02	-12337197E+02	-10873720E+03	-10729979E+03	-10527717E+03
-65251597E+01	-57179599E+01	-19354164E+01	-42599688E+01	-36208355E+01
-30753115E+01	-25910102E+01	-21634094E+01	-17868944E+01	-14176349E+01
-11665824E+01	-71510192E+00	-16000030E+01	-15556804E+01	-16017664E+01
-23308127E+00	-13561117E+00	-158729035E+01	-332393044E+02	-345497264E+01
-49831560E+01	-50101573E+01	-37116753E+01	-26693093E+02	-245497213E+01
-11437160E+00	-21493519E+01	-37318926E+01	-63921071E+01	-45497213E+01
-16946520E+01	-21493519E+01	-12888904E+01	-66342234E+01	-43681195E+01
-17703376E+01	-11323794E+01	-55278797E+01	-331503179E+00	-14452601E+01
-22920014E+01	-11742847E+01	-65271661E+00	-21113904E+01	-42612044E+01
-22626089E+01	-11513839E+01	-24771330E+01	-11042094E+01	-21441823E+01
-89031779E+00	-61138560E+00	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.

CRYs/DERI/ASIL FE(80%) = GE(20%)

18/7/77

R*V(R)

5.978707E+02	5.977604E+02	5.976049E+02	5.975224E+02	5.973940E+02
5.972507E+02	5.972070E+02	5.971644E+02	5.970829E+02	5.966449E+02
5.954577E+02	5.952109E+02	5.951675E+02	5.951080E+02	5.956798E+02
5.942459E+02	5.938143E+02	5.937714E+02	5.937199E+02	5.946362E+02
5.9302793E+02	5.9258413E+02	5.925414E+02	5.924899E+02	5.923326E+02
5.9187434E+02	5.9146714E+02	5.914245E+02	5.913729E+02	5.9128761E+02
5.9183072E+02	5.9177366E+02	5.917341E+02	5.916844E+02	5.916495E+02
5.9178480E+02	5.9172455E+02	5.916810E+02	5.916344E+02	5.915977E+02
5.9171453E+02	5.9167556E+02	5.916330E+02	5.915864E+02	5.915490E+02
5.9149320E+02	5.9145354E+02	5.914119E+02	5.913752E+02	5.913380E+02
5.9132879E+02	5.9129484E+02	5.912512E+02	5.912146E+02	5.911779E+02
5.9111307E+02	5.9107399E+02	5.9103731E+02	5.909999E+02	5.909622E+02
5.9030377E+02	5.9026731E+02	5.9023139E+02	5.901959E+02	5.901604E+02
5.9048230E+02	5.9044013E+02	5.9039813E+02	5.903629E+02	5.903273E+02
5.9020142E+02	5.9016532E+02	5.9013039E+02	5.900957E+02	5.900609E+02
5.8945055E+02	5.8941780E+02	5.893810E+02	5.893444E+02	5.893088E+02
5.8872195E+02	5.8855550E+02	5.884189E+02	5.883823E+02	5.883467E+02
5.8781203E+02	5.8760091E+02	5.874643E+02	5.873286E+02	5.872924E+02
5.8690972E+02	5.868303E+02	5.867057E+02	5.865710E+02	5.864357E+02
5.8532497E+02	5.8518750E+02	5.8505135E+02	5.849170E+02	5.847813E+02
5.8367589E+02	5.8330225E+02	5.8292613E+02	5.825315E+02	5.821433E+02
5.8169720E+02	5.814284E+02	5.8083921E+02	5.802139E+02	5.795877E+02
5.7958717E+02	5.7865296E+02	5.7833764E+02	5.7768238E+02	5.7704846E+02
5.7644452E+02	5.7619791E+02	5.7586293E+02	5.755384E+02	5.751067E+02
5.7390760E+02	5.7330213E+02	5.7293842E+02	5.7269102E+02	5.7243857E+02
5.70740118E+02	5.6967650E+02	5.6934536E+02	5.690122E+02	5.687757E+02
5.67270449E+02	5.66604495E+02	5.6620767E+02	5.658758E+02	5.647304E+02
5.6395962E+02	5.62943528E+02	5.6250442E+02	5.6217758E+02	5.616457E+02
5.6073720E+02	5.5988005E+02	5.5942998E+02	5.590404E+02	5.581281E+02
5.572273E+02	5.56323295E+02	5.5597693E+02	5.555877E+02	5.546889E+02
5.5388039E+02	5.5303011E+02	5.5262849E+02	5.521809E+02	5.515509E+02
5.503797E+02	5.4915447E+02	5.4879348E+02	5.4840667E+02	5.4792657E+02
5.4625148E+02	5.45628201E+02	5.4526677E+02	5.448971837E+02	5.435857E+02
5.429880E+02	5.4064220E+02	5.384484E+02	5.3744997E+02	5.374592E+02
5.395279E+02	5.36102557E+02	5.3420616A7E+02	5.3480197E+02	5.3557782E+02
5.3592790E+02	5.3279322E+02	5.3082988E+02	5.2973380E+02	5.2955277E+02
5.3251890E+02	5.292932E+02	5.2732657E+02	5.2559308E+02	5.249011884E+02
5.2861614E+02	5.2505172E+02	5.2306372E+02	5.2085394E+02	5.23027667E+02
5.2498635358E+01	5.2151952313E+01	5.19852212E+01	5.17923254E+01	5.12259515E+01

CRYSTALLOGRAPHY

18/7/77

ADDITIONAL VINT FOR DERILOG= 0.0000
 L'MAX= 2
 NUMBER OF ENERGIES= 60
 BOTTOM ENERGY= 0.0100
 STEP ENERGY= 0.0200

LOGARITHMIC DERIVATIVES FOR L=0 TO L=2

ENERGY	L=0	L=1	L=2
0.0100	1644287E+00	5067266E+00	5836278E+00
0.0300	1529185E+00	4970196E+00	5716192E+00
0.0500	1413185E+00	4884678E+00	5593190E+00
0.0700	1276271E+00	4792279E+00	5469296E+00
0.0900	1159643E+00	4700328E+00	5342279E+00
0.1100	977052E+00	4607546E+00	5212953E+00
0.1300	8171703E+00	4514251E+00	508027E+00
0.1500	6771752E+00	4420405E+00	4946094E+00
0.1700	5771752E+00	4329241E+00	480837E+00
0.1900	490970E+00	4231211E+00	4667066E+00
0.2100	3914767E+00	4132211E+00	433719E+00
0.2300	2914767E+00	4034266E+00	4193991E+00
0.2500	1914767E+00	3936311E+00	3970531E+00
0.2700	1119991E+00	3838311E+00	3711701E+00
0.2900	715031E+00	36512506E+00	3440971E+00
0.3100	4150151E+00	3551110E+00	3209567E+00
0.3300	2450151E+00	3455201E+00	3007967E+00
0.3500	1570518E+00	3355201E+00	2829293E+00
0.3700	1015820E+00	3255201E+00	2646735E+00
0.3900	7124337E+00	3155201E+00	2466735E+00
0.4100	5175069E+00	3155212E+00	2386735E+00
0.4300	3935996E+00	3155404E+00	22664915E+00
0.4500	1121622E+00	3055275E+00	21457618E+00
0.4700	1260696E+00	2945909E+00	20246873E+00
0.4900	1401324E+00	2745032E+00	19028139E+00
0.5100	1542733E+00	2641336E+00	1800566E+00
0.5300	1610582E+00	2537119E+00	17563417E+00
0.5500	1403023E+00	2434245E+00	1715839E+00
0.5700	1976297E+00	2328731E+00	1656873E+00
0.5900	2123667E+00	2225274E+00	17854354E+00
0.6100	2272610E+00	2115714E+00	15002992E+01
0.6300	2423065E+00	2008191E+00	2000661E+01
0.6500	2575099E+00	1929976E+00	1466618E+01
0.6700	2728712E+00	1791909E+00	14523291E+01
0.6900	2883947E+00	1681431E+00	18084279E+01
0.7100	3049899E+00	1571077E+00	1187644E+00
0.7300	3119514E+00	1459988E+00	15928441E+00
0.7500	3359880E+00	1348151E+00	12027389E+00
0.7700	3522021E+00	1235554E+00	12475279E+00
0.7900	3645931E+00	1122106E+00	13001263E+00
0.8100	3351802E+00	10004021E+00	13551050E+00
0.8300	4017951E+00	9330420E+00	14151559E+00
0.8500	4189176E+00	7773213E+00	14811255E+00
0.8700	4360812E+00	6607399E+00	15540611E+00
0.8900	4534493E+00	5433153E+00	1635273AE+00
0.9100	4710245E+00	4259427E+00	17264279E+00

.9300	-.4898123E+00	.3059048E-01	-.8296641E+00
.9500	-.5928177E+00	.1853872E-01	-.9477939E+00
.9700	-.5254459E+00	.6497513E-02	-.1284572E+01
.9900	-.5433921E+00	.5884661E-02	-.1245130E+01
.0100	-.5621920E+00	.1775934E-01	-.1436697E+01
.0300	-.5311210E+00	.3932811E-01	-.1669733E+01
.0500	-.6939453E+00	.4279257E-01	-.1969042E+01
.0700	-.6197297E+00	.5535454E-01	-.2332572E+01
.0900	-.6594036E+00	.6801524E-01	-.2629342E+01
.1100	-.6593594E+00	.8077636E-01	-.3586742E+01
.1300	-.6795680E+00	.9364101E-01	-.4580352E+01
.1500	-.7009631E+00	.10661195E+00	-.6361793E+01
.1700	-.7208431E+00	.1196842E+00	-.1003652E+02
.1900	-.7419153E+00	.1328669E+00	-.2210818E+02

PHASE SHIFTS

ENERGY	L=1	L=2
0.0100	-715553E-01	-366549E-03
0.0300	-121450E+00	-1065976E-03
0.0500	-121450E+00	-373341E-03
0.0700	-107623E+00	-839795E-03
0.0900	-256234E+00	-132746E-03
0.1100	-256234E+00	-210610E-03
0.1300	-256234E+00	-106739E-03
0.1500	-271153E+00	-106739E-03
0.1700	-271153E+00	-229262E-03
0.1900	-313559E+00	-250143E-03
0.2100	-327443E+00	-250143E-03
0.2300	-344090E+00	-324791E-03
0.2500	-350693E+00	-365953E-03
0.2700	-373929E+00	-403918E-03
0.2900	-3670617E+00	-442269E-03
0.3100	-4009412E+00	-406926E-03
0.3300	-4150119E+00	-519827E-03
0.3500	-426310E+00	-519827E-03
0.3700	-433169E+00	-590110E-03
0.3900	-450110E+00	-676110E-03
0.4100	-46110E+00	-776110E-03
0.4300	-47116E+00	-776110E-03
0.4500	-4941603E+00	-776110E-03
0.4700	-495618E+00	-776110E-03
0.4900	-595059E+00	-1542132E-03
0.5100	-5159911E+00	-8731132E-03
0.5300	-5261865E+00	-91231198E-03
0.5500	-529200E+00	-9213132E-03
0.5700	-519493E+00	-9933135E-03
0.5900	-5557217E+00	-1022197E+00
0.6100	-5952515E+00	-1067637E+00
0.6300	-571632E+00	-1102111E+00
0.6500	-5033735E+00	-11471369E+00
0.6700	-5719514E+00	-142457E+00
0.6900	-571952E+00	-1225308E+00
0.7100	-2108262E+20	-1251097E+00
0.7300	-6128587E+20	-2702011E+00
0.7500	-628374E+20	-293641E+00
0.7700	-628374E+20	-322791E+00
0.7900	-6367221E+20	-352191E+00
0.8100	-6367221E+20	-4161535E+00
0.8300	-6334695E+20	-44840316E+00
0.8500	-6046392E+20	-14810498E+00
0.8700	-697875E+20	-5672522E+00
0.8900	-6650362E+20	-253059E+00
0.9100	-5937141E+20	-1501049L+00
0.9300	-7045119E+20	-1021043L+00
0.9500	-7045119E+20	-1001041L+00
0.9700	-7045119E+20	-931044L+00
0.9900	-7344070E+20	-759111L+00
1.0100	-731293E+20	-892076L+00
1.0300	-731293E+20	-183532L+00
1.0500	-76719E+20	-186760E+00
1.0700	-7540561E+20	-1904242E+00
1.0900	-7612862E+20	-1923320E+00
1.1100	-7614646E+20	-1972215E+00
1.1300	-77553412E+20	-20028511E+00

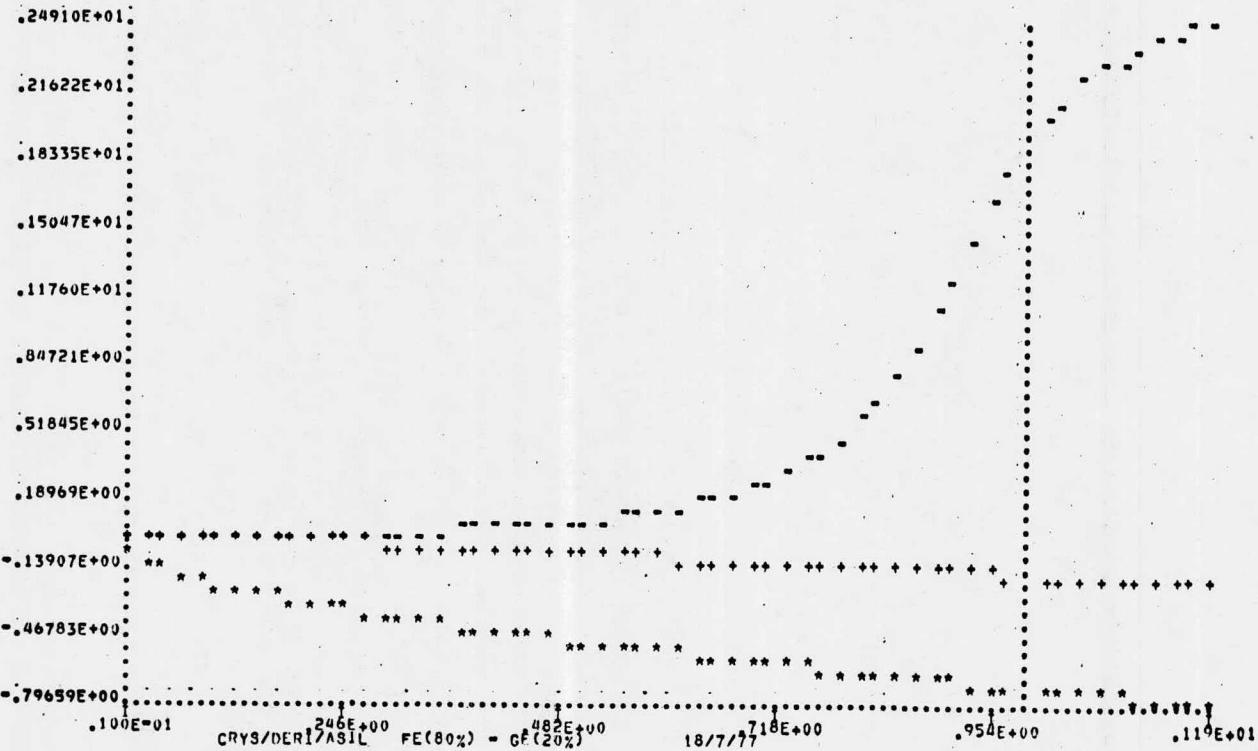
1.1500 - .7826497E+00 - .2139469E+00 - .7050315E+00
 1.1700 - .789428E+00 - .2172830E+00 - .6758866E+00
 1.1900 - .7905895E+00 - .2100019E+00 - .6505855E+00

CEP

 0.0100 - .9917257E+01 - .2514622E+04 - .4618283E+06
 0.0300 - .5730997E+01 - .4921475E+03 - .8949605E+05
 0.0500 - .4537408E+01 - .2327519E+03 - .8187974E+04
 0.0700 - .3379541E+01 - .1427504E+03 - .3513356E+04
 0.0900 - .3461816E+01 - .1055113E+02 - .1864595E+04
 0.1100 - .3160733E+01 - .7487337E+02 - .1122775E+04
 0.1300 - .279300612E+01 - .5925144E+02 - .7351095E+03
 0.1500 - .277799832E+01 - .4053611E+02 - .5108172E+03
 0.1700 - .264357121E+01 - .4492302E+02 - .3711043E+03
 0.1900 - .2525215E+01 - .3517740E+02 - .2790572E+03
 0.2100 - .2313771E+01 - .3177413E+02 - .2156845E+03
 0.2300 - .2309705E+01 - .2727674E+02 - .1794741E+03
 0.2500 - .2233032E+01 - .2445766E+02 - .1372631E+03
 0.2700 - .2232962E+01 - .2121912E+02 - .1122696E+03
 0.2900 - .2207125E+01 - .2119135E+02 - .8904807E+02
 0.3100 - .2141420E+01 - .1955542E+02 - .7799558E+02
 0.3300 - .2149620E+01 - .1715578E+02 - .6604933E+02
 0.3500 - .2192625E+01 - .1589779E+02 - .5602906E+02
 0.3700 - .2140653E+01 - .1497837E+02 - .4552703E+02
 0.3900 - .2122229E+01 - .1497839E+02 - .4205290E+02
 0.4100 - .1993537E+01 - .1342967E+02 - .3820309E+02
 0.4300 - .1968197E+01 - .1247933E+02 - .3282396E+02
 0.4500 - .1975576E+01 - .1112314E+02 - .2850833E+02
 0.4700 - .1972304E+01 - .1052163E+02 - .2507430E+02
 0.4900 - .1937219E+01 - .9785670E+01 - .2162624E+02
 0.5100 - .1931172E+01 - .9392076E+01 - .17655159E+02
 0.5300 - .1927707E+01 - .9392076E+01 - .15809316E+02
 0.5500 - .1924339E+01 - .9316146E+01 - .1418290E+02
 0.5700 - .1925651E+01 - .8393576E+01 - .1153714E+02
 0.6100 - .1928615E+01 - .8113336E+01 - .10337107E+02
 0.6300 - .1933215E+01 - .7652278E+01 - .8388344E+01
 0.6500 - .1939456E+01 - .7609908E+01 - .8492745E+01
 0.6700 - .1947322E+01 - .7384425E+01 - .7692620E+01
 0.7100 - .1956817E+01 - .7174224E+01 - .6971405E+01
 0.7300 - .1967951E+01 - .6977879E+01 - .6313290E+01
 0.7500 - .1930741E+01 - .6771185E+01 - .5672779E+01
 0.7700 - .1929523E+01 - .6622490E+01 - .5167735E+01
 0.7900 - .1911408E+01 - .6462357E+01 - .4703914E+01
 0.8100 - .1929486E+01 - .6303833E+01 - .426560344E+01
 0.8300 - .1949301E+01 - .6165297E+01 - .385264214E+01
 0.8500 - .1971104E+01 - .6030399E+01 - .341372405E+01
 0.8700 - .1994981E+01 - .5993093E+01 - .3137228E+01
 0.8900 - .2120735E+01 - .5782721E+01 - .2822474E+01
 0.9100 - .2149129E+01 - .5660862E+01 - .2533789E+01
 0.9300 - .2179692E+01 - .5561423E+01 - .2264504E+01
 0.9500 - .2212785E+01 - .5458706E+01 - .2016858E+01
 0.9700 - .2248583E+01 - .5361797E+01 - .1787372E+01
 0.9900 - .2287299E+01 - .5267622E+01 - .1574422E+01
 1.0100 - .2329145E+01 - .5182031E+01 - .1376535E+01
 1.0300 - .2374388E+01 - .5093706E+01 - .1122231E+01
 1.0500 - .2423321E+01 - .5091738E+01 - .1022555E+01
 1.0700 - .2476294E+01 - .4943816E+01 - .8602347E+00
 1.0900 - .2533688E+01 - .4871785E+01 - .7103690E+00

1.1100	=.2595958E+01	=.4803083E+01	.5700820E+00
1.1300	=.2653625E+01	=.4737521E+01	.4385882E+00
1.1500	=.2737294E+01	=.4674926E+01	.3151781E+00
1.1700	=.2817674E+01	=.4615136E+01	.1992092E+00
1.1900	=.2795545E+01	=.4558002E+01	.9009873E-01

FERMI LEVEL= 0.98222 RYDBERGS
APPROXIMATE FERMI LEVEL FOR THE ALLOY= 1.07569
VALENCE= 0.00000
FOR L = 0 PHASESHIFT AT FERMI LEVEL= -0.72151014
FOR L = 1 PHASESHIFT AT FERMI LEVEL= -0.7524632
FOR L = 2 PHASESHIFT AT FERMI LEVEL= 1.85636612



FE-GE

10/8/77

CALCULATION OF THE DENSITY OF STATES FOR COMPLEX OF

2 SCATTERERS IN

FE-GE

MAXIMUM SINGLE SITE PHASESHIFT= 2

NUMBER OF TYPES OF ATOMS 2

ATOMS PER UNIT CELL= 4.00000

LATTICE PARAMETER A= 7.05376

POINTS FOR THE INTERPOLATING FUNCTION= 4

**P ELECTRONS ACCOUNTED

ENERGY REGION: EMIN= 0.11500000 EMAX= 1.39869100 WITH STEP EDELTA= 0.03000000

PHASESHIFT USED IN CALCULATION WITH SSCE= 1.000000 PSCF= 1.000000

ATOMS TYPE 1 : VALENCE ELECTRONS= 8 NUMBER OF ATOMS= 1
ENERGIES AND PHASESHIFTS:

ENERGY	S	ENERGY	P	ENERGY	D
0.01000	-0.07166	0.01000	-0.00037	0.01000	0.00000
0.03000	-0.12142	0.03000	-0.0187	0.03000	0.00004
0.05000	-0.16042	0.05000	-0.0393	0.05000	0.00014
0.07000	-0.18937	0.07000	-0.0635	0.07000	0.00033
0.09000	-0.21524	0.09000	-0.0913	0.09000	0.00062
0.11000	-0.24204	0.11000	-0.1231	0.11000	0.00122
0.13000	-0.26886	0.13000	-0.1559	0.13000	0.00186
0.15000	-0.28815	0.15000	-0.1857	0.15000	0.00229
0.17000	-0.29652	0.17000	-0.2050	0.17000	0.00318
0.19000	-0.31480	0.19000	-0.2250	0.19000	0.00416
0.21000	-0.32644	0.21000	-0.2456	0.21000	0.00556
0.23000	-0.33500	0.23000	-0.2586	0.23000	0.00700
0.25000	-0.34500	0.25000	-0.2700	0.25000	0.00866
0.27000	-0.35907	0.27000	-0.2850	0.27000	0.01093
0.29000	-0.37393	0.29000	-0.3000	0.29000	0.01331
0.31000	-0.38766	0.31000	-0.3145	0.31000	0.01633
0.33000	-0.40094	0.33000	-0.3280	0.33000	0.01912
0.35000	-0.41381	0.35000	-0.3519	0.35000	0.02205
0.37000	-0.42631	0.37000	-0.3889	0.37000	0.02643
0.39000	-0.43847	0.39000	-0.4281	0.39000	0.03116
0.41000	-0.45032	0.41000	-0.4375	0.41000	0.04184
0.43000	-0.46187	0.43000	-0.4676	0.43000	0.05423
0.45000	-0.47316	0.45000	-0.4710	0.45000	0.06540
0.47000	-0.48420	0.47000	-0.4755	0.47000	0.07256
0.49000	-0.49501	0.49000	-0.4794	0.49000	0.08279
0.51000	-0.50560	0.51000	-0.4342	0.51000	0.09434
0.53000	-0.51520	0.53000	-0.4873	0.53000	0.10740
0.55000	-0.52619	0.55000	-0.5125	0.55000	0.12223
0.57000	-0.53620	0.57000	-0.5915	0.57000	0.13510
0.59000	-0.54604	0.59000	-0.6304	0.59000	0.15838
0.61000	-0.55572	0.61000	-0.6777	0.61000	0.18050
0.63000	-0.56525	0.63000	-0.7100	0.63000	0.20603
0.65000	-0.57403	0.65000	-0.7401	0.65000	0.23564
0.67000	-0.58387	0.67000	-0.7725	0.67000	
0.69000	-0.59278	0.69000	-0.8004	0.69000	

0.71000	-0.61082	J. 71000	-0.12581	0.71000	0.27020
0.73000	-0.61937	J. 73000	-0.12556	0.73000	0.31062
0.75000	-0.62830	J. 75000	-0.12530	0.75000	0.35008
0.77000	-0.63672	J. 77000	-0.12502	0.77000	0.41615
0.79000	-0.64514	J. 79000	-0.12471	0.79000	0.48433
0.81000	-0.65347	J. 81000	-0.12439	0.81000	0.56755
0.83000	-0.66169	J. 83000	-0.12405	0.83000	0.66723
0.85000	-0.66983	J. 85000	-0.12370	0.85000	0.76655
0.87000	-0.67703	J. 87000	-0.12331	0.87000	0.87337
0.89000	-0.68504	J. 89000	-0.12291	0.89000	1.08412
0.91000	-0.69371	J. 91000	-0.12248	0.91000	1.23323
0.93000	-0.70151	J. 93000	-0.12194	0.93000	1.42269
0.95000	-0.70923	J. 95000	-0.12158	0.95000	1.61502
0.97000	-0.71684	J. 97000	-0.12131	0.97000	1.77115
0.99000	-0.72445	J. 99000	-0.12101	0.99000	1.90661
1.01000	-0.73195	J. 101000	-0.12069	1.01000	2.02103
0.03000	-0.73938	J. 03000	-0.12035	0.03000	2.1641
0.05000	-0.74675	J. 05000	-0.12000	0.05000	2.0502
0.07000	-0.75495	J. 07000	-0.11942	0.07000	2.29156
0.09000	-0.76129	J. 09000	-0.11883	0.09000	2.31674
1.10000	-0.76846	J. 11000	-0.11722	1.10000	2.30325
1.13000	-0.77558	J. 13000	-0.11659	1.13000	2.42276
1.15000	-0.78264	J. 15000	-0.11595	1.15000	2.43656
1.17000	-0.78964	J. 17000	-0.11528	1.17000	2.45571
1.19000	-0.79659	J. 19000	-0.11460	1.19000	2.49101

ENERGY REGION: EMIN= 0.11500000 EMAX= 1.39869100 WITH STEP EDELTA= 0.03000000

PHASESHIFT USED IN CALCULATION WITH SSCE= 1.000000 PSCF= 1.000000

ATOMS TYPE 2 : VALENCE ELECTRONS= 4 NUMBER OF ATOMS= 1
ENERGIES AND PHASLSHIFTS:

ENERGY	S	ENERGY	P	ENERGY	D
0.01000	-0.53411	J. 01000	-0.00224	0.01000	0.00000
0.03000	-0.40492	J. 03000	-0.01120	0.03000	0.00001
0.05000	-0.35829	J. 05000	-0.02570	0.05000	0.00002
0.07000	-0.31771	J. 07000	-0.03304	0.07000	0.00012
0.09000	-0.30722	J. 09000	-0.03345	0.09000	0.00024
0.11000	-0.31777	J. 11000	-0.03659	0.11000	0.00049
0.13000	-0.37568	J. 13000	-0.04085	0.13000	0.00099
0.15000	-0.54383	J. 15000	-0.04508	0.15000	0.00095
0.17000	-0.60496	J. 17000	-0.04798	0.17000	0.01116
0.19000	-0.65975	J. 19000	-0.05859	0.19000	0.01144
0.21000	-0.70407	J. 21000	-0.06230	0.21000	0.0198
0.23000	-0.75673	J. 23000	-0.06295	0.23000	0.0249
0.25000	-0.80605	J. 25000	-0.067615	0.25000	0.0337
0.27000	-0.85005	J. 27000	-0.07259	0.27000	0.0373
0.29000	-0.87492	J. 29000	-0.07629	0.29000	0.0446
0.31000	-0.91408	J. 31000	-0.07606	0.31000	0.0527
0.33000	-0.91913	J. 33000	-0.07854	0.33000	0.0616
0.35000	-0.91716	J. 35000	-0.08022	0.35000	0.0714
0.37000	-0.91293	J. 37000	-0.08089	0.37000	0.0820
0.39000	-0.90278	J. 39000	-0.08239	0.39000	0.0925
0.41000	-0.87145	J. 41000	-0.08461	0.41000	0.1058
0.43000	-0.89303	J. 43000	-0.08745	0.43000	0.01190
0.45000	-0.12563	J. 45000	-0.08085	0.45000	0.01331

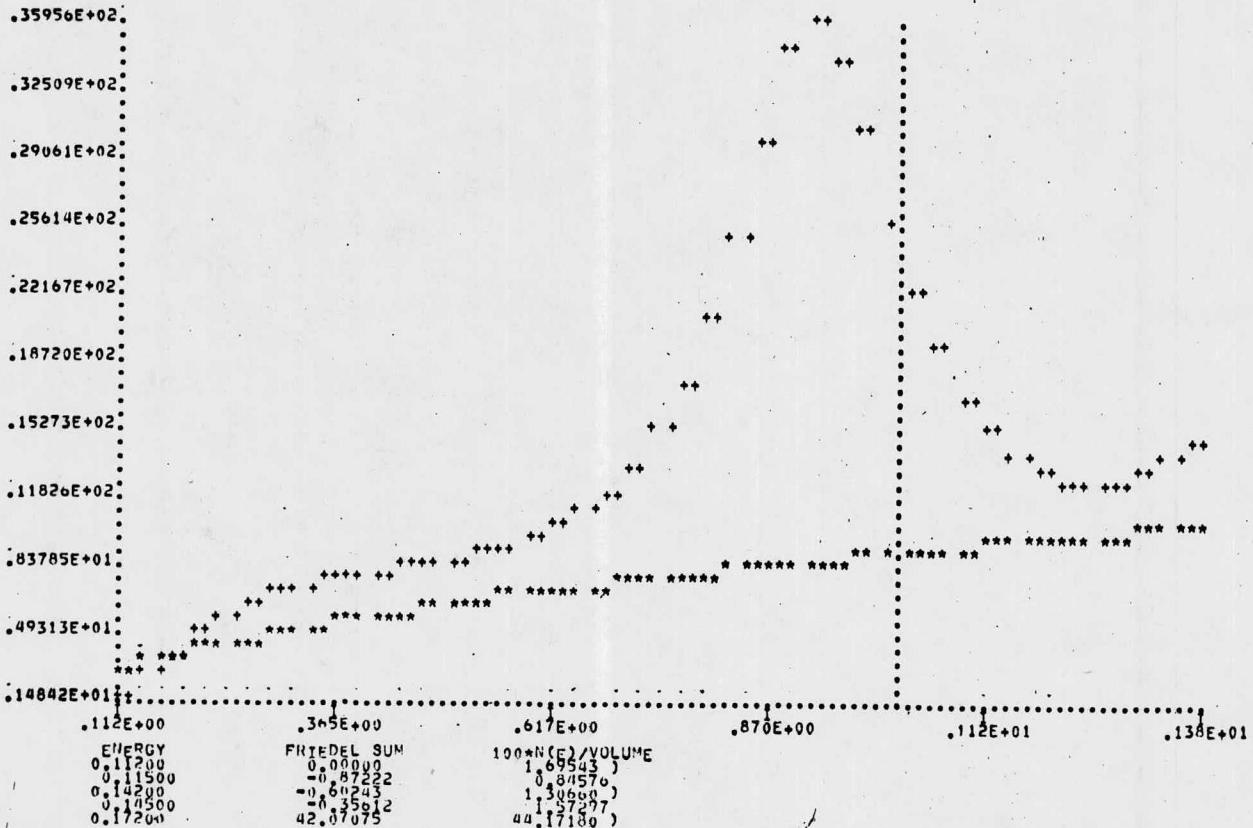
0.47000	-2.15132	0.47000	0.62478	0.47000	0.01481
0.49000	-2.17616	0.49000	0.64722	0.49000	0.01641
0.51000	-2.20023	0.51000	0.66818	0.51000	0.01649
0.53000	-2.22358	0.53000	0.68768	0.53000	0.01887
0.55000	-2.24626	0.55000	0.70577	0.55000	0.02174
0.57000	-2.26831	0.57000	0.72249	0.57000	0.02370
0.59000	-2.28877	0.59000	0.73789	0.59000	0.02576
0.61000	-2.31067	0.61000	0.75204	0.61000	0.02791
0.63000	-2.33196	0.63000	0.76499	0.63000	0.03015
0.65000	-2.35095	0.65000	0.77680	0.65000	0.03228
0.67000	-2.37025	0.67000	0.78755	0.67000	0.03442
0.69000	-2.38938	0.69000	0.79728	0.69000	0.03742
0.71000	-2.40796	0.71000	0.80696	0.71000	0.04053
0.73000	-2.42641	0.73000	0.81396	0.73000	0.04273
0.75000	-2.44159	0.75000	0.82191	0.75000	0.04551
0.77000	-2.45134	0.77000	0.82228	0.77000	0.04839
0.79000	-2.46131	0.79000	0.83203	0.79000	0.05135
0.81000	-2.47594	0.81000	0.83768	0.81000	0.05439
0.83000	-2.48120	0.83000	0.84190	0.83000	0.05752
0.85000	-2.48700	0.85000	0.84500	0.85000	0.06073
0.87000	-2.49372	0.87000	0.84726	0.87000	0.06402
0.89000	-2.50530	0.89000	0.85126	0.89000	0.06739
0.91000	-2.51702	0.91000	0.85511	0.91000	0.07084
0.93000	-2.52809	0.93000	0.85827	0.93000	0.07437
0.95000	-2.53950	0.95000	0.86157	0.95000	0.07796
0.97000	-2.55042	0.97000	0.86492	0.97000	0.08163
0.99000	-2.56145	0.99000	0.86834	0.99000	0.08537
1.01000	-2.57155	1.01000	0.87164	1.01000	0.08918
1.03000	-2.58145	1.03000	0.88595	1.03000	0.09295
1.05000	-2.59155	1.05000	0.89540	1.05000	0.09698
1.07000	-2.60165	1.07000	0.90556	1.07000	0.10098
1.09000	-2.71195	1.09000	0.85446	1.09000	0.10493
1.11000	-2.71507	1.11000	0.85312	1.11000	0.10814
1.13000	-2.72401	1.13000	0.85165	1.13000	0.11220
1.15000	-2.74075	1.15000	0.85079	1.15000	0.11621
1.17000	-2.75333	1.17000	0.84777	1.17000	0.12179
1.19000	-2.76574	1.19000	0.84500	1.19000	0.12607

LX= 0.00000 LY= 0.00000 LZ= 0.00000

LX= 0.00000 LY= 3.52688 LZ= 3.52688

ENERGY	CLUSTER CHANGE	FREE ELECTRON	DENSITY OF STATES	INTEGRATED DENS. OF STATES
0.11200	0.00003	0.97517	0.0004495	
0.11500	-1.53559	0.01475	0.0004495	
0.14200	-1.5710	0.29285	0.0872556	
0.14500	-0.2493	0.7028	0.0872556	
0.17200	73.2651	0.51345	0.0872556	
0.17500	0.10392	3.52383	0.0872556	
0.20200	0.41764	4.41320	0.0872556	
0.20500	0.70900	4.73498	0.0872556	
0.23200	0.46687	4.40880	0.0872556	
0.23500	1.20423	0.13833	0.0872556	
0.26200	1.40925	0.95068	0.0872556	
0.26500	1.59535	0.57217	0.0872556	
0.29200	1.74941	0.51777	0.0872556	
0.29500	1.68551	0.55331	0.0872556	
0.32200	1.97295	0.14030	0.0872556	
0.32500	0.08441	7.07557	0.0872556	
0.35200	2.15559	7.15253	0.0872556	
0.35500	0.03555	7.42499	0.0872556	
0.38200	2.38053	7.50030	0.0872556	
0.38500	2.63330	7.13260	0.0872556	
0.41200	2.76009	7.77940	0.0872556	
0.41500	2.87581	8.98234	0.0872556	
0.44200	2.87582	8.01079	0.0872556	
0.47500	2.99664	8.49787	0.0872556	
0.47600	2.99697	8.22908	0.0872556	
0.47900	2.99493	8.03574	0.0872556	
0.50200	2.52417	8.31495	0.0872556	
0.50500	2.55959	8.02492	0.0872556	
0.53200	2.54759	6.66844	0.0872556	
0.53500	5.25118	8.71682	0.0872556	
0.56200	0.50248	8.04080	0.0872556	
0.59500	0.68234	8.18972	0.0872556	
0.59800	0.74187	8.26009	0.0872556	
0.62500	2.87513	8.36153	0.0872556	
0.65200	2.87501	10.00404	0.0872556	
0.67500	3.64604	10.32148	0.0872556	
0.68200	3.64465	10.32148	0.0872556	
0.71200	4.21953	11.32148	0.0872556	
0.71500	4.24055	11.32952	0.0872556	
0.71700	5.10901	11.32952	0.0872556	
0.71800	5.10901	11.32952	0.0872556	
0.74200	6.47649	12.61453	0.0872556	
0.74500	7.34434	13.62440	0.0872556	
0.77200	8.52591	14.67761	0.0872556	
0.77500	9.48013	14.37017	0.0872556	
0.80200	10.41623	16.06725	0.0872556	
0.80500	12.52722	18.37765	0.0872556	
0.83200	14.47086	20.50357	0.0872556	
0.83500	16.02074	20.57978	0.0872556	
0.86200	19.00017	27.44413	0.0872556	
0.86500	21.45187	27.26201	0.0872556	
0.89200	23.78551	29.72000	0.0872556	
0.89500	25.84473	28.18124	0.0872556	
0.92200	26.93842	24.55070	0.0872556	
0.92500	27.40563	4.47266	0.0872556	
0.95200	-47.39194	34.55581	0.0872556	
0.95500	25.34132	34.07179	0.0872556	
		34.02901	0.15180	

FERMI LEVEL	0.98200	23.42490	8.00964	32.23462	11.15180
0.98200	21.28252	8.82308	30.10580	11.05496	
0.98200	16.01819	9.5319	30.96129	11.05496	
0.98200	17.80922	9.5644	32.76955	11.05496	
0.98200	14.80273	9.7478	33.97781	11.05496	
0.98200	12.92900	9.8783	32.91764	11.05496	
0.98200	11.32114	9.9149	32.52395	11.05496	
0.98200	9.76420	9.92173	32.52395	11.05496	
0.98200	8.63045	9.93539	17.87724	11.05496	
0.98200	7.53041	9.93509	10.08725	11.05496	
0.98200	6.63105	9.45057	10.08725	11.05496	
0.98200	5.81919	9.71109	10.08725	11.05496	
0.98200	5.14879	9.70003	14.72760	11.05496	
0.98200	4.55213	9.70545	14.72760	11.05496	
0.98200	4.02620	9.70930	14.72760	11.05496	
0.98200	3.58024	9.71021	14.72760	11.05496	
0.98200	3.23577	9.82730	14.72760	11.05496	
0.98200	2.94977	9.93744	14.72760	11.05496	
0.98200	2.76219	9.95076	14.72760	11.05496	
0.98200	2.53062	9.95919	14.90001	11.05496	
0.98200	2.39515	10.09755	14.90001	11.05496	
0.98200	2.14019	10.09755	14.90001	11.05496	
0.98200	1.96335	10.18384	14.90001	11.05496	
0.98200	1.79205	10.20440	14.90001	11.05496	
0.98200	1.61220	10.20861	14.90001	11.05496	
0.98200	1.45904	10.41300	14.76915	11.05496	
0.98200	1.35911	10.41300	14.76915	11.05496	
0.98200	1.31125	10.42446	14.72760	11.05496	
0.98200			14.73571	11.05496	



ENERGY	FRIEDEL SUM	100*N(E)/VOLUME
0.11200	0.00000	1.69543
0.11500	-0.87222	0.84576
0.14200	-0.60243	1.30660
0.14500	-0.35812	1.57297
0.17201	42.07075	44.17180

0.17500	0.405922	2.17850
0.20200	0.438011	2.51491
0.232500	0.40062	2.99827
0.23200	0.550982	2.99112
0.23500	0.68624	3.4211
0.26200	0.80321	3.39618
0.26500	0.90213	3.51704
0.29200	0.94623	3.73447
0.29500	1.07448	3.82605
0.322500	1.13570	4.01044
0.32500	1.18784	4.07594
0.35200	1.22553	4.2121
0.35500	1.276571	4.37417
0.38200	1.289370	4.56507
0.38500	1.29705	4.53317
0.41200	1.30145	4.636503
0.441500	1.30357	4.67608
0.441500	1.30532	4.70991
0.47200	1.30824	4.74053
0.47500	1.31349	4.78053
0.50200	1.32445	4.84288
0.50500	1.33968	4.82979
0.53200	1.36401	5.05016
0.53500	1.39460	5.10016
0.56200	1.43900	5.16885
0.56500	1.49214	5.20012
0.59200	1.56248	5.40038
0.59500	1.64411	5.625188
0.62200	1.74058	5.745160
0.62500	1.77029	6.1141
0.65200	2.02074	6.535098
0.68200	2.19991	6.583326
0.68500	2.43378	7.21522
0.71200	2.44445	7.55772
0.71500	2.44448	8.05416
0.74200	3.67398	8.53513
0.74500	3.69081	9.1956
0.77200	4.16245	9.86240
0.77500	4.74465	10.95700
0.80200	5.40254	11.80410
0.80500	6.2072	12.80731
0.83200	8.13810	14.10088
0.83500	8.4635	15.53552
0.86200	10.831080	16.93620
0.86500	10.831080	18.33879
0.89200	13.652456	19.52059
0.89500	13.652456	20.21445
0.92200	15.140697	20.48977
0.92500	15.01737	22.00578
0.95200	-2.780672	
0.95500	14.41100	16.39176
0.98200	13.44089	18.3921
0.98500	13.44089	17.5597
1.01200	10.83765	15.03401
1.01500	10.83765	14.68281
1.04200	8.73548	13.66683
1.04500	8.736817	12.64990
1.07200	6.45146	11.69673

1.07500	5.62166	10.87426
1.10200	4.32521	10.92089
1.12000	3.56635	9.12024
1.13500	3.77079	9.19864
1.16200	3.31612	8.11331
1.16500	2.82952	8.37054
1.19500	2.82950	7.82344
1.219500	2.26441	7.87823
1.222000	1.84405	7.43428
1.252500	1.68035	7.328805
1.25500	1.67406	7.24262
1.28500	1.47820	7.31495
1.28500	1.47866	7.31492
1.31200	1.48760	7.33244
1.31500	1.55363	7.35613
1.34200	1.64807	7.35749
1.34500	1.79404	7.60340
1.37200	1.97117	7.81648
1.37500	2.14915	8.13315
	2.45681	8.38729

BEGIN CALCULATION

FOR L= 0 SINGLE SITE PHASESHIFT=-1.40627 K=MATRIX=17.99761

FOR L= 1 SINGLE SITE PHASESHIFT= 0.08871 K=MATRIX=-0.26578

FOR L= 2 SINGLE SITE PHASESHIFT= 0.00041 K=MATRIX=-0.00121

REAL PART OF DET= 0.21559 IMAG PART DET 0.97648

FOR ENERGY= 0.14200 RYDBERGS
DENSITY OF STATES PER UNIT VOLUME*100 IS 0.00000

** PROCESS TIME=133.6667 SECONDS **

FOR L= 0 SINGLE SITE PHASESHIFT=-1.41848 K=MATRIX=19.21055

FOR L= 1 SINGLE SITE PHASESHIFT= 0.09239 K=MATRIX=-0.27324

FOR L= 2 SINGLE SITE PHASESHIFT= 0.00043 K=MATRIX=-0.00128

REAL PART OF DET= 0.20454 IMAG PART DET 0.97801

FOR ENERGY= 0.14200 RYDBERGS
CHANGE IN DENSITY OF STATES IS -1.53059 0.84570

DENSITY OF STATES PER UNIT VOLUME*100 IS ** PROCESS TIME=139.4167 SECONDS **

FOR L= 0 SINGLE SITE PHASESHIFT=-1.51757 K=MATRIX=49.80884

FOR L= 1 SINGLE SITE PHASESHIFT= 0.12772 K=MATRIX=-0.34079

FOR L= 2 SINGLE SITE PHASESHIFT= 0.00074 K=MATRIX=-0.00196

REAL PART OF DET= 0.16450 IMAG PART DET 0.98638

FOR ENERGY= 0.14200 RYDBERGS
CHANGE IN DENSITY OF STATES IS -1.05716 1.30660

DENSITY OF STATES PER UNIT VOLUME*100 IS ** PROCESS TIME=145.2167 SECONDS **

FOR L= 0 SINGLE SITE PHASESHIFT=-1.52756 K=MATRIX=60.70236

FOR L= 1 SINGLE SITE PHASESHIFT= 0.13187 K=MATRIX=-0.34833

FOR L= 2 SINGLE SITE PHASESHIFT= 0.00078 K=MATRIX=-0.00204

REAL PART OF DET= 0.16159 IMAG PART DET 0.98686

FOR ENERGY= 0.14200 RYDBERGS
CHANGE IN DENSITY OF STATES IS -0.62493 1.57297

DENSITY OF STATES PER UNIT VOLUME*100 IS ** PROCESS TIME=151.0000 SECONDS **

FOR L= 0 SINGLE SITE PHASESHIFT=-2.87178 K-MATRIX=-0.23611
FOR L= 1 SINGLE SITE PHASESHIFT= 0.81943 K-MATRIX=-0.91391
FOR L= 2 SINGLE SITE PHASESHIFT= 0.16684 K-MATRIX=-0.14377
REAL PART OF DET= 0.97301 IMAG PART DET 0.24668
FOR ENERGY= 1.37200 AYDJOGS
CHANGE IN DENSITY OF STATES IS 3.85911
DENSITY OF STATES PER UNIT VOLUME*100 IS 8.13315 ** PROCESS TIME=657.5167 SECONDS **

FOR L= 0 SINGLE SITE PHASESHIFT=-2.87344 K-MATRIX=-0.23433
FOR L= 1 SINGLE SITE PHASESHIFT= 0.81893 K-MATRIX=-0.91200
FOR L= 2 SINGLE SITE PHASESHIFT= 0.16753 K-MATRIX=-0.14422
REAL PART OF DET= 0.97301 IMAG PART DET 0.22694
FOR ENERGY= 1.37500 AYDJOGS
CHANGE IN DENSITY OF STATES IS 4.31125
DENSITY OF STATES PER UNIT VOLUME*100 IS 8.39729 ** PROCESS TIME=664.2167 SECONDS **

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TABLA I

	Vint	$E_f - Vint$	E_f	$\delta_2(E_f)$	$\frac{10\delta_2(E_f)}{\pi}$
γ -Fe($4s^2 3d^6$)	-1.56654	0.33177	-1.2348	2.16463	6.89
Co($4s^2 3d^7$)	-1.20163	0.22072	-0.9809	1.79127	5.702
Co($4s^{1.2} 3d^{7.8}$)	-1.1007	0.39178	-0.70892	2.54519	8.101
Ni($4s^2 3d^8$)	-1.87469	0.8400	-1.03469	2.48024	7.895
Ni($4s^{0.5} 3d^{9.5}$)	-1.73218	1.27769	-0.4545	2.38156	7.581
Ni($4s^{1.1} 3d^{8.9}$)	-1.75294	1.1977	-0.55524	2.45791	7.824
Cu($4s^1 3d^{10}$)	-1.03169	0.60801	-0.4237	2.96977	9.453
Rh($5s^1 4d^8$)	-1.31644	0.56726	-0.74918	2.5804	8.214
Ag($5s^1 4d^{10}$)	-1.28978	0.97301	-0.3168	2.68937	8.561
Nd($6s^2 4f^3 5d^1$)	-0.59364	0.09765	-0.49599	0.31623	1.007
Eu($6s^2 4f^6 5d^1$)	-0.52504	0.26204	-0.263	0.31956	1.017
Cd(BCC) ($6s^2 4f^7 5d^1$)	-0.70768	0.22315	-0.48453	0.32006	1.019
Cd(HCP)	-0.58137	0.15863	-0.4227	0.3074	0.979
Lu($6s^2 4f^{1.4} 5d^1$)	-0.70568	0.26963	-0.43605	0.32673	1.04
Os($6s^2 5d^6$)	-1.15239	0.59506	-0.5573	2.31636	7.373
Ir($6s^2 5d^7$)	-1.17929	0.69577	-0.4835	2.51113	7.993
Pt($6s^1 5d^3$)	-1.75704	1.540	-0.2170	1.8947	6.031
Au($6s^1 5d^{10}$)	-1.29552	1.18999	-0.1055	2.42109	7.707

TABLA II

	$E_{\max \delta_2}$	$\max \delta_2(E)$	$\frac{10\delta_2(E)}{\pi}$	Carácter d deslocalizado
γ -Fe ($4s^2 3d^6$)	0.75	2.97063	9.456	0.544
Co ($4s^2 3d^7 \cdot 8$)	0.43	3.04212	9.683	0.317
Co ($4s^{1.2} 3d^7 \cdot 8$)	0.99	2.9810	9.489	0.511
Ni ($4s^2 3d^8$)	1.4	2.86412	9.1168	0.883
Ni ($4s^{0.5} 3d^{9.5}$)	1.78	2.71532	8.643	1.357
Ni ($4s^{1.1} 3d^{8.9}$)	1.30	2.77482	8.83252	1.16748
Cu ($4s^1 3d^{10}$)	0.75	2.98933	9.515	0.485
Rh ($5s^1 4d^8$)	0.85	2.69862	8.590	1.41
Ag ($5s^1 4d^{10}$)	1.03	2.69203	8.569	1.431
Nd ($6s^2 4f^3 5d^1$)	0.23	2.80740	8.936	1.064
Eu ($6s^2 4f^6 5d^1$)	0.60	2.08798	6.646	3.354
Gd (BCC) ($6s^2 4f^7 5d^1$)	0.63	2.33133	7.421	2.579
Gd (HCP)	0.41	2.55707	8.139	1.861
Lu ($6s^2 4f^{14} 5d^1$)	0.81	2.29097	7.292	2.708
Os ($6s^2 5d^6$)	0.89	2.49638	7.946	2.054
Ir ($6s^2 5d^7$)	0.89	2.54975	8.116	1.884
Pt ($6s^1 5d^9$)	1.78	2.02806	6.456	3.544
Au ($6s^1 5d^{10}$)	1.33	2.42919	7.732	2.268

TABLA III
RAZON DE OCUPACION.

$$\frac{10\delta_2(F_f)}{\pi} \quad / \quad \frac{10\delta_2(E)}{\pi}$$

$\gamma\text{-Fe}(4s^2 3d^6)$	0.72864
$\text{Co}(4s^2 3d^7)$	0.58887
$\text{Co}(4s^{1.2} 3d^{7.8})$	0.85373
$\text{Ni}(4s^2 3d^8)$	0.86598
$\text{Ni}(4s^{0.5} 3d^{9.5})$	0.87713
$\text{Ni}(4s^{1.1} 3d^{8.9})$	0.88582
$\text{Cu}(4s^1 3d^{10})$	0.99348
<hr/>	
$\text{Rh}(5s^1 4d^8)$	0.95623
$\text{Ag}(5s^1 4d10)$	0.99907
<hr/>	
$\text{Nd}(6s^2 4f^3 5d^1)$	0.11269
$\text{Eu}(6s^2 4f^6 5d^1)$	0.15302
$\text{Cd(BCC)}(6s^2 4f^7 5d^1)$	0.13731
Cd(HCP)	0.12029
$\text{Lu}(6s^2 4f^{14} 5d^1)$	0.14262
<hr/>	
$\text{Os}(6s^2 5d^6)$	0.92788
$\text{Ir}(6s^2 5d^7)$	0.98484
$\text{Pt}(6s^2 5d^8)$	0.93417
$\text{Au}(6s^1 5d^{10})$	0.99677

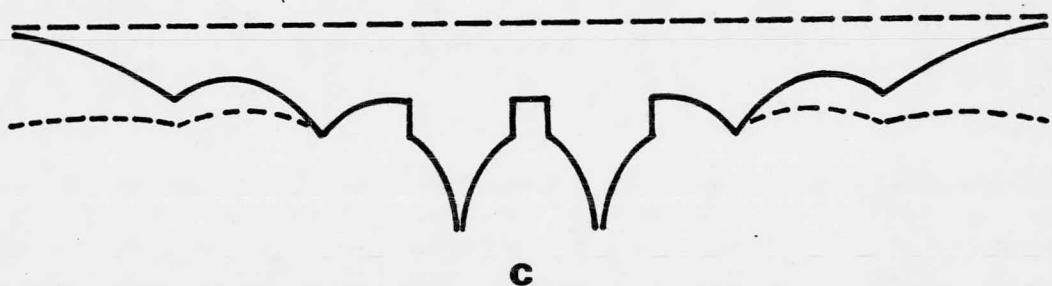
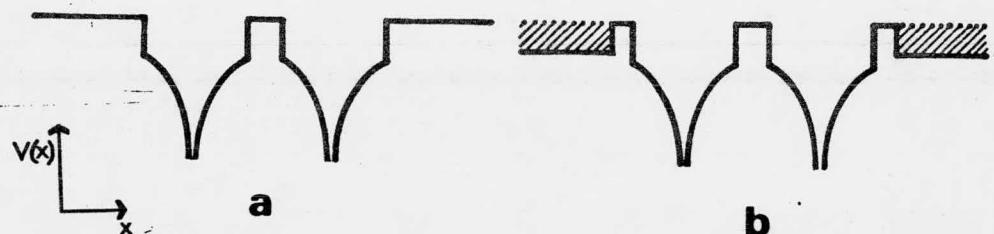


FIGURA 1

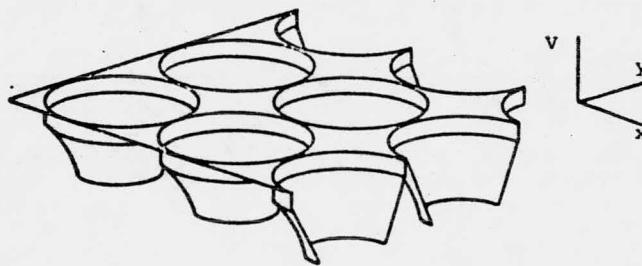


FIGURA 2

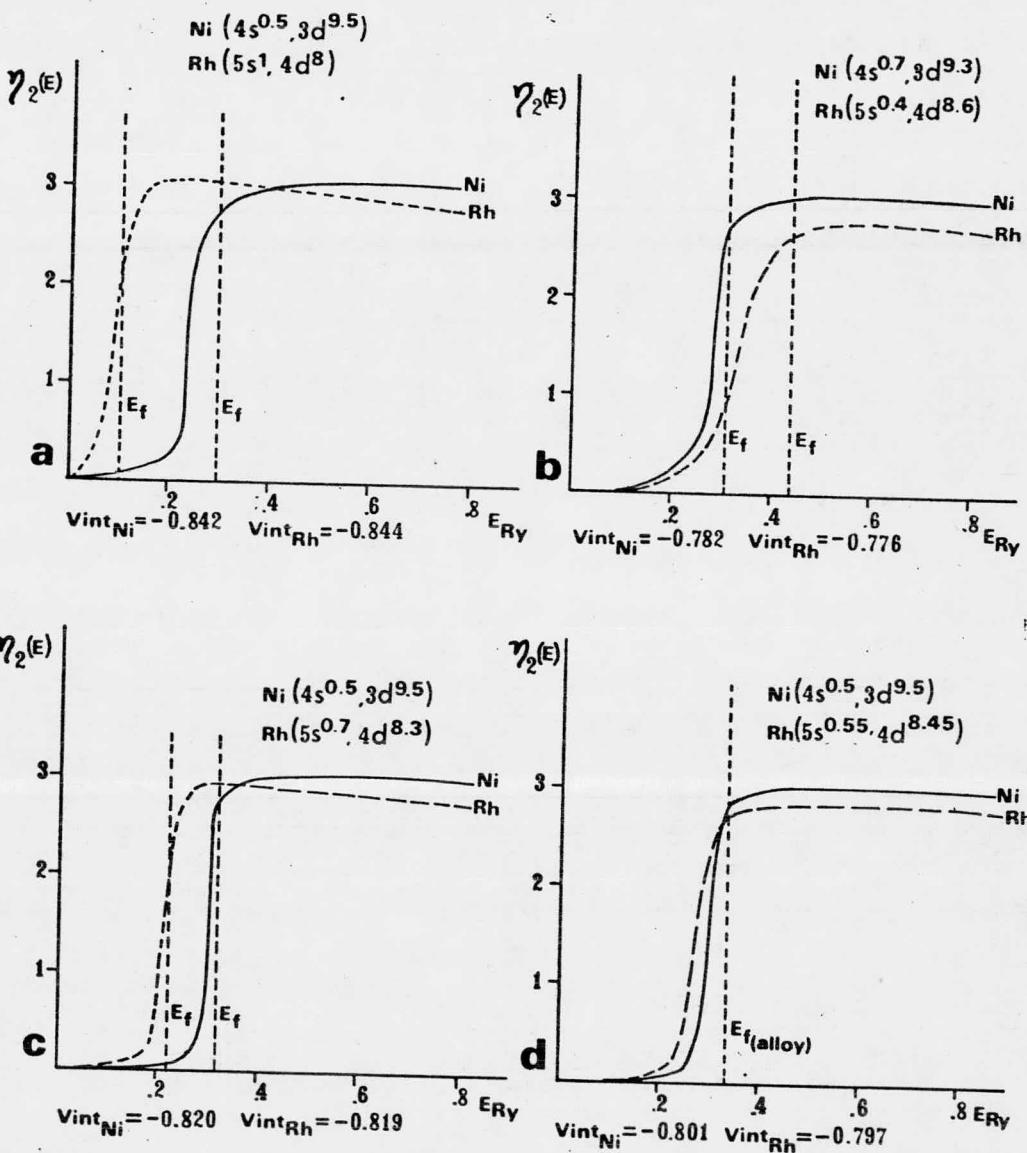


FIGURA 3

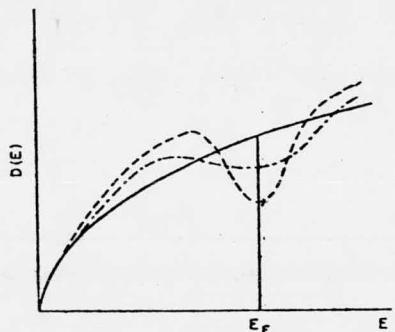


FIGURA 4

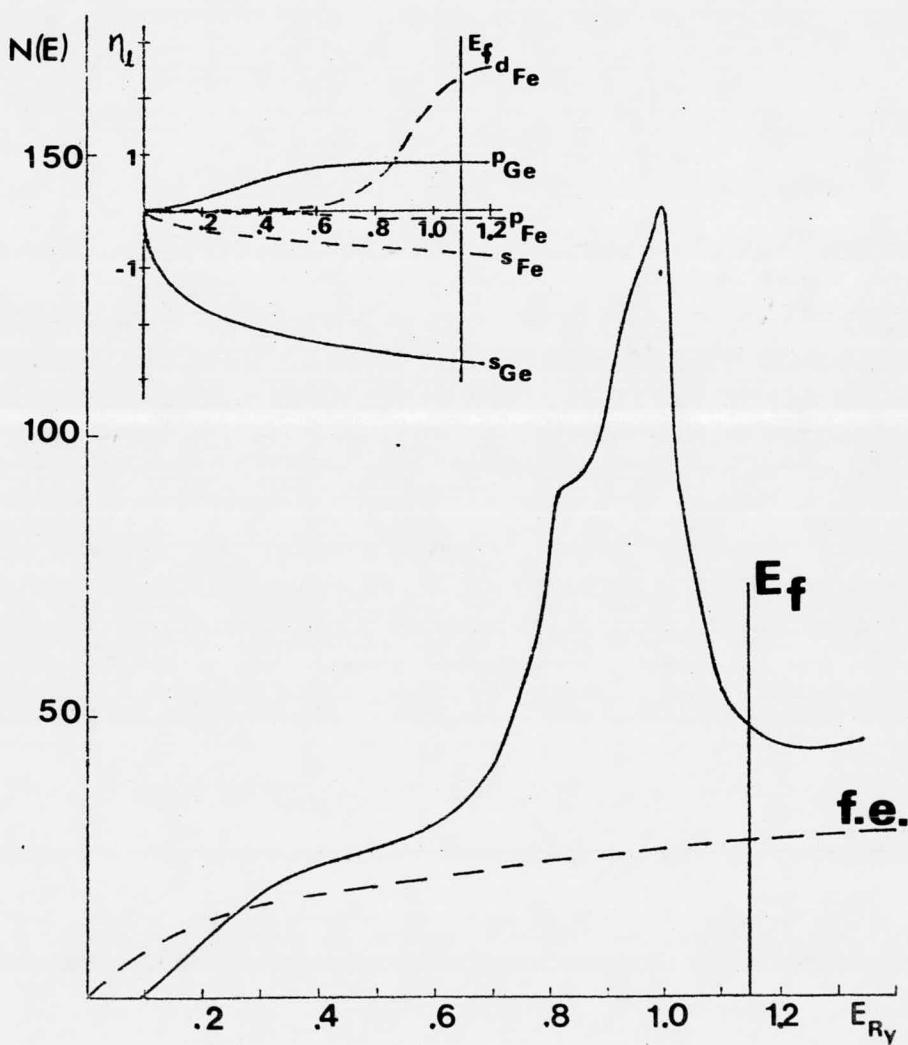


FIGURA 5

DESCRIPCION DE LAS FIGURAS.

FIG. 1.- Esta es la representación para tres aproximaciones de las condiciones a la frontera de un cúmulo de átomos en materia condensada. a) Representa a un cúmulo en el potencial intersticial V_{int} . b) Un cúmulo rodeado por el promedio del resto del sistema. c) El cúmulo rodeado por el promedio esférico del resto del sistema, la línea continua es el potencial en un sistema finito y la línea punteada en un sistema extendido.

FIG. 2.- Potencial de muffin-tin para un cristal bidimensional.

FIG. 3.- Estudio de los corrimientos de fase de la aleación Ni-Rh (50%-50% atómico). Partiendo de la ocupación óptima del Ni y del estado basal del Rh los niveles de Fermi para el Ni y el Rh son inconsistentes (a). Una disminución del carácter 3d para el Ni y un aumento del carácter 4d para el Rh no resuelve la discrepancia (b). Solo el incremento de carácter 4d en el Rh da un nivel de Fermi consistente para ambos componentes (c) y (d).

FIG. 4.- Diagrama esquemático de la densidad de estados presentado por Nagel y Tauc³² para 3 casos: La curva continua es para el modelo de electrones libres, la curva a rayas es para el vidrio en el modelo de electrones casi libres que presentan y la de la curva punteada-rayas es para un vidrio perturbado con un factor de estructura no esférica-

mente simétrico.

FIG. 5.- Densidad de estados para la aleación Fe-Ge con un contenido de 20% atómico de Ge, la línea punteada es la contribución de electrones libres. En la parte superior izquierda se presentan los corrimientos de fase para cada especie en la aleación.

86700/37700 FORTRAN COMPIILATION MARK 2.8.060

FILE 4=PERF,UNIT=PRINTER 00001000
 FILE 5= DATOS ,UNIT=READER 00002000
 FILE 6=PAPEL,UNIT=PRINTER 00003000
 FILE 7=TARJ,UNIT=PRINTER 00004000
 FILE 8=HEXD,UNIT=DISK,RECORD=14,BLOCKING=15,AREA=150*1 00005000
 FILE 9=HEXD1,UNIT=DISK,RECORD=14,BLOCKING=15,AREA=150*1 00006000
 FILE 1=HEXD2,UNIT=DISK,RECORD=14,BLOCKING=15,AREA=150*1 00007000
 FILE 11=HEXD3,UNIT=DISK,RECORD=14,BLOCKING=15,AREA=150*1 00008000
 FILE 12=HEXD4,UNIT=DISK,RECORD=14,BLOCKING=15,AREA=150*1 00009000

COMMON/CRYDER/BGX(17250),ME(20),JRI(2),OMA,ANJJ,EFE,IAL,IZZ,
 DIMENSION 1AB(250,14),SIGN(550,2),B50(250,2),W(250,2),AA(250,14),
 2AB(250,14),ACR(250),ABC(250),XNA(14,2),AD(14,2),
 3SH(4,15),XAD(3,15),SH(500,2),AAD(14,2),FAP(250),
 4SYB(14),BD(14),IZZ(2),RHE(421),RAP(250),JEC(14),XRI(2),
 5DIMENSION 1GE(250),GRAD(250),GRAD2(250),SCP(250),AA1(250),AB1(250)
 1,ACC(250,2),AE(250,2),R(2)
 REAL JP1
 FU(A,B,C,D-T)=A*(D-T)-B*(C-T)/(D-C)

E FORMAT
 28 FORMAT(1H1,30X,F10.4,/,30X,B0('*)) 00021000
 29 FORMAT(1H1,10X,701,10X,MESH PRINTS= ',I4,10X,'NUMBER OF TYPES O 00023000
 30 1E ATOMS= ',I4,10X,'NUMBER OF ATOMS FOR FCC, BCC, DIAMOND AN 00025000
 31 D, HCP) 00027000
 32 FORMAT(1H1,30X,'DISTANCE/STDE FOR FCC,BCC AND DIAMOND') 00028000
 33 FORMAT(1DX,6F16.5) 00029000
 51 FORMAT(3FI10.6) 00030000
 61 FORMAT(20A4) 00031000
 86 FORMAT(2I5) 00032000
 81 FORMAT(14I5) 00033000
 115 FORMAT(15E15.8) 00034000
 117 FORMAT(2X,VIN= ',F17.8,',LAT= ',I3,/,Z'= F10.2,',F10.7,JP1(1)= ',F10.6,', 00035000
 117(2)= ',F10.6,',XALPHA= ',F10.7,XBETA= ',F10.7, 00036000
 130 FORMAT(1H1,5X,'NEIGHBOR DISTANCES AND NUMBER OF NEIGHBORS ---CENT 00037000
 1RAL ATOM OF TYPE---',I2) 00038000
 141 FORMAT(2F10.5) 00039000
 147 FORMAT(8E14.7) 00040000
 148 FORMAT(1H1,30X,'TABLE OF APRO RADIUS') 00041000
 151 FORMAT(1H1,30X,'INTERPOLATED TABLE OF 4*PI*(P**2)*RHO FOR THIS PRO 00042000
 1GRAM, FOR THE ',I3,' ATOM') 00043000
 312 FORMAT(2X,'CENTRAL ATOM OF TYPE 11//,2X,22(I1)) 00044000
 314 FORMAT(2X,'CENTRAL ATOM OF TYPE 21//,2X,22(I1)) 00045000
 350 FORMAT(3(2E15.5,3X)) 00046000

800 FORMAT(' INTEGRAL OF CHARGE DENSITY FOR THE ',I2,' ATOM',F16.8) 00047000
 801 FORMAT(1H1,10X,'APPROXIMATE RADIUS FROM HEX= ',F10.5,10X,'RECIPROCAL OF 00048000
 1 MESH INTERVAL FROM HEX= ',F10.5,/) 00049000
 1001 FORMAT(1H1,10X,'LATTICE STRUCTURE= ',I4,/,20X,'MESH POINT CORRESPONDING TO THE APOLOSPHERE RADIUS= ',F10.6,/,20X,'VOLUME PER ATOM(ATO 00050000
 2'MC UNITS)= ',F10.6,/,20X,'LATTICE CONSTANTS A AND C',2F10.6,/,19X, 00051000
 3'EXCHANGE COEFFICIENTS ALPHA AND BETA',2F10.6,/) 00052000
 1170 FORMAT(2X,'RESULTS FOR AUFFEL TIN WITH RI(1)= ',F7.4,5X,'RI(2 00053000
 1)= ',F7.4,5X,'RI(3)= ',F7.4,5X,'V BOUNDARY= ',E14.7) 00054000
 1180 FORMAT(29X,'R*V(R)') 00055000
 9997 FORMAT(29X,'R*V(R)')

C START
 3 READ(5,80,END=310,DATA=310)ICALL,ATID
 IF(ICALL.GT.0,0) CALL ASIL(ICALL)
 80 80 TE=1,3
 50 READ(5,51,DATA=51,I0=3)(XAD(I,J),J=1,14)
 51 75 I=1,14
 75 READ(5,51)(XAD(I,J),J=1,14)
 PEND(5,51,I0=310)I0=0
 C STOP IF A CARD WITH END (PRINTED ON 2ND COLUMN) IS FOUND 00058000
 00059000
 00060000
 00061000
 00062000
 00063000
 00064000
 00065000
 00066000
 00067000
 00068000

```

C      TEC(1A) IF(JJ=1,14) READ(RHO)
C      TEC(2A) IF(JJ>14) READ(RHO)
C
C      RMAX=4*XMAX READ FROM HEX
C      NSIG=NUMBER OF SIGN POINTS FROM HEX
C      JJ=NUMBER OF TYPES OF ATOMS
C      IZZ(J)=ATOMIC NUMBER OF EACH TYPE OF ATOM
C
C      READ(S,81) RMAX,H
C      READ(S,81) NSIG,H
C      READ(S,81) IZZ,JJ
C      READ(S,81) RMAX,JJ,J=1,NJJ
C      WRITE(S,1180)
C      WRITE(S,32)
C      DO 31 I=1,3
C      31 WRITE(S,35)(XAN(I,J),J=1,14)
C      WRITE(S,1180)
C      WRITE(S,30)
C      DO 751 I=1,4
C      751 WRITE(S,81)(MAC(I,J),J=1,14)
C      WRITE(S,1180)
C      WRITE(S,30)
C      WRITE(S,35) RMAX,H
C      WRITE(S,29) NSIG,H,I,IZZ(JJ),JJ=1,NJJ
C
C      CALCULUS OF HEX AND A.P.D. MESHES
C
C      XHEX=(NSIG/H)
C      DHEX=1/H
C      DO 142 K=1,NSIG
C      142 RHEX(K)=RMAX*EXP(XHEX+K*DHEX)
C      DO 143 K=1,250
C      143 RAPW(K)=EXP(-8.8+(K-1)*0.05)
C      WRITE(S,148)
C      WRITE(S,1180)
C      WRITE(S,147)(RAPW(K),K=1,250)
C      DO 998 JJ=1,NJJ
C
C      TF(JJ,E1,20) N1=NT+KIND
C
C      STGN(J, JJ)= TABLE OF 4*PT*(P**2)*RHO FROM HEX
C      READ(MM,6) (STGN(J, JJ), J=1,NSIG)
C      DO 144 K=1,250
C      DO 145 KK=1,NSIG
C      IF(RHEX(KK)=RAPW(K))145,146,146
C      145 CONTINUE
C      146 FU1=FU2(STGN(KK, JJ),STGN(KK-1, JJ),RHEX(KK),RAPW(K))
C      FU2=FU2(STGW(KK+1, JJ),STGN(KK, JJ),RHEX(KK+1),RAPW(K))
C      147 PSQ(J, JJ)=FU1(FU2,MM,RHEX(KK+1),RAPW(K))
C      998 CONTINUE
C      DO 149 JJ=1,NJJ
C      WRITE(S,151) JJ
C      WRITE(S,1180)
C      WRITE(S,147)(PSQ(J, JJ),J=1,250)
C
C      149 CONTINUE
C      DO 996 JJ=1,NJJ
C      SUMA=0.0
C      ZZ=IZZ(JJ)
C      DO 92 JL=1,224,2
C      TSC=EXP(0.05)
C      TSC2=EXP((JL-1)*0.05-8.8)
C      92 SUMA=SUMA+TSC2*(2.0*PSQ(JL,JJ)+TSC*PSQ(JL+1,JJ))
C      SUMA=SUMA/0.033333
C      WRITE(S,148)
C      WRITE(S,1180)
C      DO 93 JL=1,224
C      93 PSQ(JL,JJ)=PSQ(JL,JJ)*ZZ/SUMA
C      DO 94 JL=225,250
C      94 PSQ(JL,JJ)=0.0
C      996 CONTINUE
C
C      LATTICE CALCULATIONS
C
C      LAT1=FCC
C      LAT2=BCC
C      LAT3=DIAMOND STRUCTURE
C      LAT4=MCP
C      LAT5=SPECIAL STRUCTURES OF ELEMENTS
C      LAT6=ALLOYS
C
C      READ(S,81)LAT
C      READ(S,99) LTR(JJ),JJ=1,NJJ
C      99 FJ2MAT(UF10,50)
C      READ(S,51) SPA,A,C,XALPHA

```

IF A IS SET TO 0.0 THEN A=1.0 IS TAKEN AND THE DISTANCES GIVEN.
IN ADD ARE 10 MORE RELATIVE DISTANCES

IF XALPHA IS NOT SPECIFIED, XALPHA-BETA EXCHANGE POTENTIAL IS CALC
WITH ALPHA=2/3 AND BETA=2.003
IF XALPHA IS GIVEN, XALPHA EXCHANGE POTENTIAL IS CALCULATED WITH T
SPECIFIED VALUE OF XALPHA

IF(XALPHA.LT.0.0)1 GO TO 1
XBETA=0.0

GO TO 4

1 XBETA=0.003

2 XALPHA=0.6666667

4 IF(LAT.0.0)1 A=1.0
WRITE(6,102)LAT,JPI(1),DMA,A,C,XALPHA,XBETA
IF(LAT-4)R2,40J,101

C C HCP CRYSTAL STRUCTURE

400 R=C/A

BS=3*B

R(1)=0

R(2)=1./3.+BS/4.

R(3)=1.-BS/4.

R(4)=4./3.+BS/4.

R(5)=BS

R(6)=7./3.+BS/4.

R(7)=3.

R(8)=1.+BS

R(9)=4.

R(10)=1./3.-BS/4.

R(11)=3.+BS

R(12)=1./3.+(7.*BS)/4.

R(13)=1./3.-BS/4.

R(14)=BS

R(15)=1./3.

2 AD(I,1)=RAD(I,1)

GO TO 52

C C FCC, BCC, AND STMNG STRUCTURES

X3 D3 T3 I,1

53 AD(I,1)=RAD(LAT,T)

52 D3 T3 I,1

X3 A(I,1)=RAD(I,1)

BS=2

23 AD(I,1)=EDG*AD(I,1)

GO TO 53

C C SPECIAL CRYSTAL STRUCTURES

614(I,1) FOR I=1,7 ARE THE NUMBER OF NEIGHBORS OF TYPE 1.
(CENTRAL ATOM). I=7 SEVEN SHELLS. FOR I=8,14 ARE THE NUMBER OF
NEIGHBORS OF TYPE 2. I=7 SEVEN SHELLS(MAY BE DIFFERENT OF THOSE
OF THE FIRST TYPE). THERE IS A RESTRICTION, SEE NEXT COMMENT.

RAD(I,1) FOR I=1,7 ARE THE RELATIVE DISTANCES OF THE SEVEN
SHELLS OF NEIGHBORS OF TYPE 1. EACH NUMBER WAS GIVEN BEFORE.
FOR I=8,14 ARE THE DISTANCES OF SECOND TYPE ATOM'S
RESTRICTION: I=8 AND (I,7)=RAD(I,14)

LAST SHELL MUST BE OF THE SAME FOR BOTH TYPE OF ATOMS.

FOR XRAD(I,2) AND RAD(I,2) CENTRAL ATOM IS OF TYPE 2. IN THE FOR
INSTINCTION I AND 2 MUST BE INTERCHANGED

101 D3 D3 T3 I,1 J3

DEAD(I,1)=RAD(I,1)

DEAD

```

9940  WRITE(6,511)(X(K,J),J=1,14)          00237000
      WRITE(6,1180)                               00280000
      GO TO 216                                 00390000
C     "OFFICE TIME SEGMENT"                   00440000
C
      65 DO 1021 JJ=1,14                      00443000
      66 K=1,14 J=1,14                         00445000
      X(K,J)=X(K,J)                           00448000
1020  RUM(K)=RUM(K)                           00450000
      WRITE(6,151)(RUM(K),K=1,14)              00450000
      WRITE(6,511)(RUM(K),K=1,14)              00470000
      WRITE(6,1180)                           00480000
      216 DO 95 K=1,14 J=1,14                  00490000
      Z=I27(JJ)                                00490000
      XC=CHI(JJ)
      CALL P015(JJ,PSQ,Z,JC,J,I,JJ)           00490000
      XC=-8.8                                     00493000
      DO 102 J=1,JC+1                          00495000
      CE=EXP(-Z**2)-2.*Z*CE+AC(J,JJ)          00497000
      AC(J,JJ)=CE*{ -2.*Z*CE+AC(J,JJ)}        00497000
C
C     (ATOMIC ELECTROSTATIC POTENTIAL)
C
      102 L(J,JJ)=PSL(J,JJ)*EXP(-Z**2)          00500000
      L(*,1)=0.010412 ELECTRONIC DENSITY       00500000
C
      100 X=X+1.5                                00523000
      200 CONTINUE                                 00564000
      IF(L(AI-5) .LT. 160) 160,160,161         00565000
160   DU 207 J=1,14                            00566000
      TK=J
      TF(JJ,E2,I,J,K)=TK=I                     00567000
      DO 215 J=1,14 JJC=1,14                   00568000
      DO 216 J=1,14 JJC=1,14                   00569000
      AA(J,J)=AAC(J,J)                         00571000
      203 DO 205 K=1,14 AAC(J,J)=AAC(J,J)        00572000
      DO 210 K=8,14 AAC(J,K)=AAC(J,J+TK)        00573000
      210 AAC(J,K)=AAC(J,J+TK)                  00574000
      215 AB(J,K)=AAC(J,J+TK)                  00575000
      209 CONTINUE                                 00576000
      DU 215 J=1,14                            00577000
      RD(K)=AAC(K,JJ)                         00578000
213   XNB(K)=XNA(K,JJ)                       00579000
      TNA1=0.0
      TNA2=0.0
      DO 215 K=1,6 TNA1=TNA1+XNB(K)           00581000
      215 TNA2=TNA2+XNB(K+7)                   00583000
      TNA1=TNA1+0.5*XNB(7)                     00584000
      TNA2=TNA2+0.5*XNB(14)                   00585000
      216 DO 163 J=1,25
      160 DU 163 K=1,14
      AAC(J,KJ)=AC(J,I)
      163 AB(J,KJ)=AE(J,1)
      MM=0
      JJ=1
102   Z=I27(JJ)
      IF(IJJ.EQ.2) GO TO 212
      DU 71 J=1,2
      XI(J)=(-8.8+0.05*(JRI(J)-1.))
      RI(J)=EXP(XI(J)))
      71  RD=((3./4.)*RMA/3.141593)**(1./3.)
      IF(LAT.GT.5) GO TO 212
      NEXT CARD MUST BE CHANGED IF DIFFERENT AVERAGE POTENTIAL IS WANTED 00303000
      JT0P=JJCHI
      XJJCHI=JT0P
      XJT0P=-8.8+0.05*(XJJCHI-1.)
      PT0P=EXP(XJT0P)
      TNA1=((4./3.)**3*141593*RT0P**3)/RMA 00305000
      CI=3./((4./3.)**3*RMA**3*I(1)**3)        00310000
      GO TO 211
      FOR SPECIAL CRYSTAL STRUCTURES THE INTERSTITIAL POTENTIAL IS 00313000
      CALCULATED BY AN INTEGRATION UP TO THE SEVEN SHELL OF NEIGH 00315000
      BOURS SPECIFIED IN AAD 00316000
      THAT IS WHY RD(7) IS USED IN NEXT CARD. 00317000
      212 JT0P=20,* ALOG(RD(7))+8.85
      PT0P=RD(7)
      CI=3.7*(ST0P**3-(TNA1*RT(1)**3+TNA2*RI(2)**3)) 00318000
      00319000
      00320000
      00321000

```

```

211 CP=2.*((P1/(2.*3.*1.11563)*2.)*2.)*(1./2.)
C** CALL SUMAX(X125A,AACR(JTOP),X125B,BD,JTOP)
C** X125EPT1(125A,(AACR(JTOP)),X125B,BD,JTOP)
C** CALL SUMAX(X125B,AACR(JTOP),X125C,CB,JTOP)
C** X125EPT1(125B,(AACR(JTOP)),X125C,CB,JTOP)
C**34 FORMAT(10X,0,14.7)
C
C BEGIN CALCULUS OF AVERAGE POTENTIAL
C
I=(LAT,LE,S1,GO,TJ,411
ARTOP=AACR(JTOP),AACR(JTOP+1),RAPW(JTOP),RAPW(JTOP+1),RTOP)
BRTOP=FR(CP(JTOP)),AACR(JTOP+1),RAPW(JTOP),RAPW(JTOP+1),RTOP)
FRC=C1*RTOP**3*RTOP
FRO=C1*RTOP**3*RTOP
FLC=C1*RAPW(JTOP)**3*AACR(JTOP)
FLD=C1*RAPW(JTOP)**3*AACR(JTOP)
VINT1=0.025*(FRC+FLC)
VINT2=0.025*(FRO+FLD)
C** WRITE(6,1122)VINT1,VINT2,LAT
C** WRITE(6,1122)ARTOP,BRTOP,JTOP
C**22 FORMAT(10X,2F11.7,2X,14)
411 VINT1=0.0
VINT2=0.0
JXB=0
XJXB=-8.85
7 JXR=JXP+1
JJRI=IFIX(JR(JJ))
IF(JXB-JJRI)5,118,5
5 XJB=XJB+0.05
IF(JXB-JTOP)120,119,119
120 FRC=C1*EXP(3.*(XJB+0.05))*AACR(XJB+1)
FRD=C1*EXP(3.*(XJB+0.05))*ABCR(XJB+1)
FLC=C1*EXP(3.*XJB)*AACR(XJB)
FLD=C1*EXP(3.*XJB)*BCR(XJB)
VINT1=VINT1+0.025*(FRC+FLC)
VINT2=VINT2+0.025*(FRD+FLD)
C**
C** VINT3=VINT1/C1
C** VINT4=VINT2/C1
C** WRITE(6,1123)VINT3,VINT4
GO TO 7
118 GGE=(AACR(JJR+1)-AACR(JJRT))*(JJR(JJ)-JJRI)
FLC=(AACR(JJR+1)+GGE)*C1*EXP(3.*XRI(JJ))
PFI1=(CP+FLC)*(XRI(JJ)-(XJB+0.05))/2.
PI1C=V1*V1*PFI1
GGE=(ABC(JJR+1)-ABC(JJRI))*(JJR(JJ)-JJRI)
FLD=(ABC(JJR+1)+GGE)*C1*EXP(3.*XRI(JJ))
PFI2=(PD+FLD)*(XRI(JJ)-(XJB+0.05))/2.
PI1E=V1*V1*PFI2
GRTEPI1=2
VRI=(4./3.)*3.141593*(R1(JJ)**3)
VEX=4.*3.141593*(R1(JJ)**3)
WRITE(6,1123)PI1C,P1,URI,VRI,VEX,C1,CP,TNA1,TNA2
C** WRITE(6,1124)PI1C,P1,URI,VRI,VEX,TNA1,TNA2
1124 FORMAT(60X,'INTEGRAL OF POTENTIAL IN THE MUFFIN TIN SPHERE',E13.6
1/,20X,'INTEGRAL OF 4*PI*RHO*',E13.6/,20X,'CHARGE INTO THE SPHERE'
E13.6/,20X,'INTEGRAL OF 4*PI*RHO*',E13.6/,20X,'EXCHANGE POTENTIAL',E13.6/
325X,'NUMBER OF ATOMS OF TYPE 1',E13.6/,20X,'EXCHANGE POTENTIAL',E13.6/
4YPE=2.,E13.6)
WRITE(6,1180)
C**23 FORMAT(7E13.6)
1123 FORMAT(7E13.6)
GO TO 5
1124 IF(LAT,ST,5) GO TO 214
VINT=VINT1-10*MA*PI1C-CP*XALPHA*VEX**((1./3.))
GO TO 216
214 VINT1=VINT1+VINT1
VINT2=VINT2+VINT2
IF(JJ,E1.2) GO TO 220
C
C STORAGE OF THE DATA OBTAINED WHEN THE CENTRAL ATOM IS OF TYPE 1
C
P1=PI1C
VINC=VINT1-TNA1*PI1
TN2=TNA2
VEX1=VEX
DO 219 J=1,JJCH1
AA1(J)=AACR(JJ)
219 AB1(J)=ABCR(JJ)
GO TO 227
221 VEXJ=(VEX1+VEX1)/2.
SIGN1=1.
TF(VEXJ-L.E.J-0.05)SIGN1=-1.
IF(TF(VEXJ-L.E.J-0.05))FORMAT(10X,14.7)
4401 FORMAT(2X,10F14.7),14X,14F14.7)
C
C EXCHANGE PART OF THE INTERSTITIAL POTENTIAL NEG

```

```

1ATIVE')
VEXC=(SIGN*VEX0)*((1./3.)
VINTATE=7INC-THP*PI10-CP*XALPHA*VEXC*SIGN
VINT =VINT1-TMA2*PI1-TMA1*PI1C-CP*XALPHA*VEXC*SIGN
207 MM=1

C BEGIN XALPHA-BETA
C
216 N=1
DO 413 J=1,JTOP
413 ABCR(J)=ABCR(J)/(4.*3.141593)
IF(XBETA.LT.1.E-05)GO TO 203
CALL DGT3(RAPM,GRCP,GRAD,JTOP,C011)
CALL DGT3(RAP1,GRAD,GRAD1,JTOP,C012)
203 DO 201 K=1,JTOP
GRAPW(K)
PJ=ABCP(K)
IF(RJ.GT.1.E-06.RJ.XBETA.GT.1.E-05) GO TO 202
ALPALB=1
GO TO 201
202 GR=GRAD(K)/RJ
QB=RJ*((1./3.)
GE(K)=((4./3.)*GR*GR-2.*((GRAD2(K)+2.*GR*RJ/Q)/RJ)/(QB*QB)
ALPALP1=+TAN((XBETA/XALPHA)*GE(K))
WRITE(6,112)RJ,GRAD(K),GRAD2(K),GE(K),ALPALP
201 SCP(K)=CP*XALPHA*ALPALP
DO 112 J=1,JTOP
ABCR(J)=ABCR(J)*4.*3.(41593
112 BGXMT(J)=ABCR(J)-SCP(J)+ABCR(J)**(1./3.)-VINT
WRITE(6,28)(NAME(I),I=1,26)

C CALCULUS OF V BOUNDARY BY INTEGRATION OF THE FINAL POTENTIAL
C IN A VOLUME PER ATOM
C CALL TRAPEZ(P0,UGXMT,VB)
C VBOUND=VB/(4*3.141593*PO**3)
C
IF(LAT.LE.5) GO TO 313
IF(MM.EQ.1) GO TO 311
WRITE(6,312)
GO TO 313
311 WRITE(6,314)
313 WRITE(6,117)RT,RU,VBOUND
WRITE(6,117)VINT,Z,(JRT(JJ),JJ=1,2),LAT,XALPHA,XBETA
WRITE(6,115)BGXMT
DO 72 K=1,250
72 BGXMT(K)=-BGXMT(K)
WRITE(6,28)NAME
WRITE(7,28)NAME
DO 73 K=1,250
73 WRITE(7,43)BGXMT(K),BGXMT(K+3),BGXMT(K+6),BGXMT(K+9),BGXMT(K+12),B
1GXMT(K+15)
74 FORMAT(10X,6F13.5)
WRITE(6,9997)
DO 1133 J=1,225
1133 FAP(J)=(BGXMT(J)+VINT)*RAPW(J)
WRITE(6,115)(FAP(J),J=1,225)
WRITE(6,1180)
IF(LAT.LE.5) GO TO 315
DO 221 J=1,JTOP
221 ABCR(J)=AB1(J)
IF(MM1.EQ.1) N=2
VINT =VINT1
Z=IZZ(1)

315 CALL LODGER(N)
MM=MM+1
IF(MM.EQ.2) GO TO 216
GO TO 3
316 STOP
THESE FINAL CARDS MAKE ZERO THE NUMBER OF NEIGHBOURS AND, IF
THE COMMENT ON CARD MM=1 (BEFORE LABEL 503) IS RELEASED, THEN
A CALCULUS IS MADE FOR THE ATOM ALONE. THIS CALCULUS OF POTEN
TIAL MUST BE SIMILAR TO ONE MADE BY HARTEE-FOCK OR HEX.

END
SUBROUTINE POISON(P30,Z,J,N,JJ)
DIMENSION P30(P50,P),N(250,2),E(250),F(250)
A=1.-0.025/48.
B=-5.-0.025/48.
FDL=EXP(-0.25)
GE=.0025/6.
C2=.9/4.

```

```

      F(1)=0
      F(1)=EXP(-.25)
      XE=-.25
      T1=0.5
      DO J=1,100
      K1=J+1
      K2=K1+1
      E=2.*F(K1)*F(K2)*(X1,J1)+1.4*PSO(T,J1)+PSO(K2,J1)/EDL
      F(J)=E/F(K2)
      X=X+.25
      H(J,J1)=2.*Z*EXP(-.5*x)
      DO G=1,100
      JV=G-J1
      JV1=JV+1
      H(JV,J1)=E(JV)+W(JV1,J1)/F(JV)
      RETURN
      END

      SUBROUTINE CHIAT(JCHIAT,CHICRY,JJCCHI,XRA,AD,JTCP)
      DIMENSION CHIAT(250,14),CHICRY(250),XRA(15),AD(15),STOR(250,15)
      SUBS OVER 14 ARE FIRST SHELLS OF ATOMS
      XJJCHI=JJCHI
      TBLX=.05*(XJJCHI-1.)-8.8
      DO G=1,100
      STOR(G,1)=CHIAT(G,1)
      JA=G
      7 X=-8.8
      I=1
      8 X1=T
      ET=EXP(X)
      PLX=ALOG(ABS(AD(JA)-ET))
      IF (TBLX-TBLX)9,.50,.50
      9 JBL=2.+20.*{BLX+R(.8)
      XJBL=JBL
      XBL=.05*(XJBL-1.)-8.8
      GEXBL=BLX
      X1UT=EXINT+.5*G*(CHIAT(JBL,JA)*(2.+20.*G)*EXP(2.*XBL)+20.*G*CHIAT(
      1,JBL-1,JA)*EXP(2.*{XBL-.05)))
      TLX=ALOG(AD(JA)+ET)
      10 IF (TLX-TBLX)10,11,11
      11 JTLE=JJCHI
      GO TO 40
      12 JTLE=1.+20.*{TLX+8.8
      AF=(JTLE-JBL)12,.13,.13
      FZ1=CHIAT(JTLE,JA)*EXP(2.*{XBL-.05))
      FZ2=CHIAT(JTLE,JA)*EXP(2.*{XBL))
      FZ1=FZ1+20.*{FZ2-FZ1)*({BLX-XBL+.05}
      X1UT=.5*(FZ1+FZ2)*(TLX-BLX)
      GO TO 50
      13 XJTL=JTLE
      XTL=.05*(XJTL-1.)-8.8
      C=TLX-XTL
      K3=7*T+.17+.5*C*(CHIAT(JTL,JA)*(2.+20.*C)*EXP(2.*XTL)+CHIAT(K3,JA)*
      12.*C*EXP(.5*(XTL+.05)))
      14 X1UT=X1UT+.5*(CHIAT(JBL,JA)*EXP(2.*XBL)+CHIAT(JBL+1,JA)*EXP(2.*(
      1*(XBL+.05)))*.05
      JBL=JBL+1
      IF (JBL-JTLE)15,.50,.50
      15 XBLE=XBL+.05
      GO TO 16
      16 STOR(1,JA)=-.5*X1UT*XRA(JA)/LNU(JA)+ET
      IF (I-JTLE)16,17,17
      17 I=I+1
      X=X+.05
      GO TO 8
      18 IF (JA-14)18,20,20
      19 JA=JA+1
      GO TO 7
      20 I=1
      21 JA=1
      CHICRY(1)=0
      22 CHICRY(1)=CHICRY(1)+STOR(I,JA)
      IF (JA-14)23,24,24
      23 JA=JA+1
      GO TO 22
      24 IF (I-JTLE)25,26,26
      25 I=I+1
      TI=I-1

```

```

      GO TO 21
      RETURN
      END

      SUBROUTINE UGTR(X,Y,Z,IUTR,IER)
      DOUBLE PRECISION X(1),Y(1),Z(1)
      IER=-1
      IF(IUTR=3)B1,B1
      1 A=X(1)
      B=Y(1)
      I=2
      DY=X(2)-A
      IF(DY<0.5)DY2
      2 DY2=(Y(2)-B)/DY2
      DO 3 I=3,IUTR
      A=X(I-1)
      B=Y(I-1)
      IFC(I-3)=DY2
      3 Z(I)=DY1+DY3-DY2
      4 Z(I-1)=DY1+DY2-DY3
      IER=0
      5 I=IUDT1
      6 Z(I)=DY2+DY3-DY1
      7 RETURN
      8 IEP=I
      9 IET=I
      IF(I>2)B8,B7
      B7
      SET C111
      SUBROUTINE LOGPER()
      LOGARITHMIC DERIVATIVES SUBROUTINE. ALSO COMPUTES PHASE SHIFTS.
      SIMPLIFIED VERSION
      COMMON/CRYDER/AGX(CPSL),TEXT(24),JRI(2),UMA,A0,UJJ,EFF,TAL,IZZ
      DIMENSION ISTER(6),P(5,60),PP(5,90),Y(260),AN(5,90)
      1 FFG(5),CHD(5),F(5),CFG(5),ELTA(5,70),CFP(5,60)
      DIMENSION DFD(5,60),PINT(5,60),DVINT(5,70),CF(4)
      REAL JRI,JR1
      INTEGER NUMA(2),ZVAL(2)

      SYMBOLS TO PLOT
      DATA ISTER/1,1,1,1,*1,1+1,1-1,1+1/
      MAXL=MAXIMUM ANGULAR MOMENT
      NEN=NUMBER OF ENERGIES
      STEP=STEP ENERGY
      DVINT=ADDITIONAL V INTERSTITIAL
      ZVAL=NUMBER OF VALENCE ELECTRONS
      FU(A,B,C,D,T)=(A*(C-T)-B*(D-T))/(C-D)
      *READ(5,10)MAXL,NE,ZVAL(1),ZVAL(2),NUMA(1),NUMA(2),BE,ES,DVINT(1),
      1 DVINT(2),IPRESIS
      1 FUMAT(615,4F10.5,215)

      AGX=CONDENSED MATTER POTENTIAL (MUFFIN-TIN)
      DO 2 T=1,23
      2 AGXT(T)=AGX(1)+DVINT(T)
      WRITE(6,3)TEXT
      3 WRITE(6,4),T,20X,2DN4)
      WRITE(6,4),DVINT(1),MAXL,BE,ES
      4 FORMAT(//,20X,'ADDITIONAL VINT FOR DERILOG=',F10.4,/,20X,'LMAX=',2
      12X,/,20X,'NUMBER OF ENERGIES=',14,/,20X,'BOTTOM ENERGY=',F10.4,/,2
      20X,'STEP ENERGY= ',F10.4)

      NUMERICAL SOLUTION OF SCHRÖDINGER EQUATION. MILNE'S METHOD
      JRI=JRI(1)
      NACE=353535E-01
      DB=DAC*10.1

      NL=MAXL+1
      DO 5 I=1,NL
      NL=I
      GEML=0.5)**2
      ERBL=ES

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```

DO S J=1,JE
EEF+FS
EJ(J)=E
YJ'1=E-2D
YJ=EXP(-5*(JL+D)*YJ'1)
SG'1=+EXP(-17.5*(AGX(1)-E))
SG=0+EXP(-17.5*(AGA(2)-E))
X=-0.9
Y(1)=JRI
Y(2)=YJ
JJPI=FIX(JRI)
DO o K=1,JJRI+1
X=X+0.05
EEF=EXP(2.*{X+0.05})
SGP1=0+LEF*(AGX(K+2)-E)
A=1-DAC*SGP1
B=-2.-DB*SG
C=1.-DAC*SG,11
YJP1=(B*YJ+C*YJ'1)/A
Y(K+2)=YJP1
YJ=YJP1
SGM1=SG
SG=0+SG
6 SG=0+SG
XJ=-0.95
R=RADIAL PART OF THE WAVE FUNCTION
RPBDERIVATIVE OF P
YJF=UF(YJRI),Y(JJRI+1),JJPI,JJRT+1,JRI)
P(I,J)=EXP(-0.5*(-8.85+0.15*JRF))YJRI
YP1=(Y(JJRT-2)-8.0*Y(JJRT-1)+8.0*(Y(JJRT+1)-Y(JJRT+2))/0.6
YP2=(Y(JJRT-1)-8.0*Y(JJRT)+8.0*Y(JJRT+2)-Y(JJRT+3))/0.6
YP=UF(YP1,YP2,1,JPI,JRT)
PP(I,J)=EXP(-1.5*(-8.85+0.05*JRI))*(YP=0.5*YJRI)
C AN=LOGARITHMIC DERIVATIVES
5 ANC(I,J)=PP(I,J)/P(I,J)
WRITE(6,7)'AXL'
7 FORMAT(4(/),20X,'LOGARITHMIC DERIVATIVES FOR L=0 TO L=',I1)
WRITE(6,8)
8 FORMAT(13X,'E,ENRGY',8X,'L=0',11X,'L=1',11X,'L=2',11X,'L=3')
9 WRITE(6,9)
10 FORMAT(10X,E10.4,4E10.4)
11 FORMAT(14,20X,'PHASE SHIFTS ',/,21X,12('*'))
12 FORMAT(6,3) DO 14 J=1,JE
13 FORMAT(14,20X,'PHASE SHIFTS ',/,21X,12('*'))
14 FORMAT(6,3) DO 14 J=1,JE
15 DO 12 I=1,L
E=EI(J)
CALL OLDASH(E,JRI,1AXL,CLD,CFG,FLD,FFG)
TETA=CFG(I)*(CLD(I)-AI(I,J))/(FFG(I)*(FLD(I)-AN(I,J)))
8 ELTA=PHASESHIFTS
ELTA(I,J)=ATAN(TETA)
CET =COS(ELTA(I,J))/SIN(ELTA(I,J))
12 CEP(I,J)=CET -FFG(I)/CFG(I)
WRITE(6,16)I,J,ELTA(I,J),I=1,L)
WRITE(6,17)
282 FORMAT(20X,'CEP',/,21X,3('*'))
11 WRITE(6,18) E=EI(J),(CEP(I,J),I=1,L)
281 FORMAT(10,20X,'ENERGY',8X,'L=0',11X,'L=1',11X,'L=2',11X,'L=3')
C THIS PART OF THE PROGRAM MAKES THE PHASESHIFTS CONTINUOUS
DO 21 K=1,NL
ISIGN=1
10 J=1
DO 21 J=1,JE
IF(JLT.0)DIF=ABS(ELTA(K,J+1)-ELTA(K,J))
GO TO(9,19,21),I0
19 ELTA(K,J)=ELTA(K,J)+ISTG*3.141593
20 IF(DIF>LT.1.0) GO TO21
ID=ID+1
IF(ELTA(K,I).LT.0.0) ISIGN=-1
21 CONTINUE
FORMAT(20X,'VALENCE',F10.6)
C CALCULUS OF THE FLUX LEVEL BY FRIEDEL SUM
EEF2=EEF*(IJ(J-1))
10 I=1
DO 22 J=1,JE
22

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OMEGA=0.1A*(EN(J)*((3./P_))/((3*3.141593**2))
SUMAEU,J=1,NL
IF(N.EQ.4)GO TO 23
SUMAEU=(P*(K-1)+1)*ELTACK,J)/3.141593+SUMA
23 CONTINUE
SIGMA=OMEGA+SUMA
RESTA(1)=SIGMA-ZVAL(1)
IF(RESTA(1).GE.1E-3) IOUT=-3
IF(CJ.T.2) IOU=1,IOUT+1
IF(IOUT.EQ.0) GO TO 124
24 CONTINUE
EFE=INTER(EN,RESTA,NE,0,0,4)
WRITE(6,279) EFE
EFF2=(PF2+EFE)**/FLOAT(NJJ)
IF(N.EQ.1 AND NJJ.EQ.2) WRITE(6,283) EFE2
WRITE(6,227) ZVAL(R)
C DO 25 I=1,NL
DO 26 J=1,NE
26 CF(I,J)=INTER(IZZ,IEN,NE,EFE,4)
25 WRITE(6,280) I,I,CF(I,J)
IF(PESIS.GT.0) CALL RESIS(OMA,EFE,IZZ,CF,N)
C PLOTTING PHASESHIFTS
CALL CARTE(NE,ELTA,EN,ISTER,NL,EFE)
WRITE(6,215) TEXT
IF(CAL.EQ.20) RETURN
NPHE
TEG(J,EQ.2) GO TO 29
EMAX=EFCP+1.3
NPHE=(ENMAX-UF)/ES+1
NPHEMIN=(NPHE,1)
IF(NJJ.EQ.1) GO TO 28
REWIND IAL
DO 27 I=1,NL
DO 27 J=1,NE
27 READ(IAL,278) AN(I,J),AN(I,J+1),AN(I,J+2),AN(I,J+3),AN(I,J+4),AN(I,J+5),AN(I,J+6),AN(I,J+7)
28 REWIND IAL
WRITE(IAL,277) AN,RE,EMAX,ES,MAXL,NPH,NJJ,NUMA(1),ZVAL(1),NUMA(2),
*ZVAL(2)
277 FORMAT(4F10.5,7I3)
WRITE(IAL,278) EN(K),K=1,NPH
29 DO 31 K=1,NL
30 WRITE(IAL,278) (ELTACK(K,J),J=1,NPH)
IF(NJJ.EQ.1) CALL ASIL(IAL)
IF(N.EQ.2.0P,TAL.EQ.0) RETURN
WRITE(IAL,278) (EN(K),K=1,NPH)
DO 31 K=1,NL
31 WRITE(IAL,278) (AN(K,J),J=1,NPH)
CALL ASI(IAL)
278 FORMAT(4F10.5)
279 FORMAT(//,20X,'FERMI LEVEL=',F10.5,' RYDBERGS')
280 FORMAT(20X,'FOR L=',F12.8,' PHASESHIFT AT FERMI LEVEL='F12.8)
283 FORMAT(20X,'APPROXIMATE FERMI LEVEL FOR THE ALLOY='F10.5)
C 15 FORMAT(1H ,20X,20A4)
C RETURN
$RESET OWN
END
SUBROUTINE TRAPEZ(R0,BGXMT,VINT)
DIMENSION RGXMT(PSU)
ARO=20*(8.85+ALUG(R0))
JRO=ARO
PI4=4.*3.141593
JXB=0
XJXB=-8.85
7 JXB=JXB+1
IF((JXB-JRO)>0.05)
5 XJXB=XJXB+0.05
FR=PI4*EXP((XJXB+0.05)*3.141593*BGXMT(JXB+1))
FL=PI4*EXP((3.*XJXB)*BGXMT(JXB))
VINT=VINT+0.025*(FR+FL)
GO TO 7
6 ARGO=BGXMT(JRO)+(BGXMT(JRO)+BGXMT(JRO+1))*(ARO-JRO)
FL=PI4*EXP((3.*ALUG(R0))*BGXMT(JRO))
END=0.025*(FP+FL)
VINT=VINT+FL
RETURN
END
00742000
00743000
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SUBROUTINE BLDASH4(CE, JRI, LMAX, CLU, LFG, FLD, FFG)
  DIMENSIONI BLD(10), BFG(10), CLD(10), CFG(10), FLD(10), FFG(10), ELD(10),
  1 FFG(10)
  DOUBLE PRECISION BLD, BFG, CLU, A, PS, X, BJMO, BJZ, Z, P, Q, ZMULT, ZC, ELD,
  1 FFG, XJRI, XI
  REAL JPI
  ENEE
  XJPI=JPI
  XI=0.95*(XJPI-1.)-8.8
  P50UEXP(XI)
  NLD=LMAX+2
  NNN=NLD-1
  PEE2.
  Q=1.0
  A=DSORT(DABS(EN))
  X=A*RS
  IF(EN)<5.27.51
  5 BJMO=-IMAGINAGY(BJZ)-PFAL
  BJMO=5.5*(DEXP(-X)+DEXP(X))/X
  BJZ=-0.5*(DEXP(-X)-DEXP(X))/X
  C=-1.0
  GO TO 52
  51 BJMO=DCOS(X)/X
  BJZ=DSIN(X)/X
  C=1.0
  52 ZC=C
  BFG(1)=BJZ
  BFG(2)=ZC*(BJZ/X-BJMO)
  EFG(1)=-BJMO
  EFG(2)=-ZC*(BJMO/X+BJZ)
  DO 70 I=2,NLD
  Z=I
  ZMULT=ZC**I
  EFG(I+1)=ZMULT*(P*Z-Q)*BFG(I)/X-EFG(I-1)
  70 EFG(I+1)=ZMULT*(P*Z-Q)*EFG(I)/X-EFG(I-1)
  BLD(1)=-BFG(2)
  ELD(1)=-EFG(2)
  DO 71 I=1,NLD
  Z=I
  BLD(I+1)=(Z*BFG(I)-(Z+Q)*BFG(I+2))/(P*Z+Q)
  71 ELD(I+1)=(Z*EFG(I)-(Z+Q)*EFG(I+2))/(P*Z+Q)
  DO 72 I=1,NLD
  Z=I
  ZMULT=ZC**I
  BLD(I)=(BLD(I)/BFG(I))*A*ZMULT
  ELD(I)=(ELD(I)/EFG(I))*A*ZMULT
  CLD(I)=BLD(I)
  CFG(I)=BFG(I)
  FLD(I)=ELD(I)
  72 FFG(I)=EFG(I)
  GO TO 28
  27 WRITE(0,73)
  73 FORMAT(14H ZERO ENERGY )
  28 RETURN
  END
  REAL FUNCTION INTER(Y,X,N,Z,NPP)
  DIMENSION Y(6),X(6),FU1(10)
  FU1(A,B,C,D,T)=(A*(D-T)-B*(C-T))/(D-C)
  DO 1 KUAL=1,N
  1 AF(1)=X(KUAL)12,2,1
  CONTINUE
  2 TU=KUAL-NPP/2
  IF(TU.LT.1) TU=1
  IF(NPP+10.GT.N) TU=N-NPP+1
  L=IU
  DO 3 J=1,NPP
  FU1(J)=Y(L)
  3 L=L+1
  4 IX=1
  P=0.5*K=(NPP+1)
  FU1(K)=FO(FU1(K),FU1(K+1),X(IU),X(IU+IX),Z)
  5 IU=IU+1
  TU=L-NPP
  IX=IX+1
  IF(IX.LT.NPP) GO TO 4
  INTER=FU1(1)
  RETURN
  END
  SUBROUTINE CARTE(C,X,T,IS,NEF)
  DIMENSION X(5,100),T(100),IS(6),XPL(100),XPO(100),IG(5,100),
  1 L(100),A(6)
  20 FORMAT(14H,E14.0)
  21 FORMAT(2X)

```

```

22 FOPEN(1H1)
24 FOPEN(15X,B('I
25 FORMAT(1H+,E1.14,1D+1)) )
26 FORMAT(1H+,14X,1D+1)) )
27 FORMAT(1H+,14X,1D+1))
28 WRITE(6,22)
29 CALL MIMAX(T,T0,TF,I)
30 DO 1 K=1,I
31 DO 2 J=1,I
32 XPL(J)=X(K,J)
33 CALL MIMAX(XPL,XMIN,XMAX,I)
34 XPL0(K)=XMIN
35 KK=K+I
36 XPL0(KK)=XMAX
37 KK=2,*I
38 CALL MIMAX(XPL0,XMIN,XMAX,KK)
39 DO 4 K=1,51
40 DO 42 J=1,I
41 TG(2,J)=50.*((1.-(X(K,J)-XMIN)/(XMAX-XMIN))+1.5
42 DO 4 K=1,51
43 L(1)=IS(1)
44 DO 5 J=2,101
45 L(J)=IS(5)
46 DO 6 I=1,I
47 IF(I.GT.I-1)-K)7,8,7
48 SJ=100.*((I-1)/(I-1)+1.5
49 JJ=SJ
50 L(JJ)=IS(I+2)
51 CONTINUE
52 JK=((TF-T0)/(TF-T0))*100+1.5
53 IF(JKL.GT.101) GO TO 77
54 L(JKL)=IS(1)
55 WRITE(6,301)(L(KK),KK=1,101)
56 DO 6 KK=1,101
57 L(KK)=IS(2)
58 CONTINUE
59 IF(K=51)17,18,17
60 SJ=(K+4)/5.
61 JK=SJ
62 IF((JK-SJ)>19.9
63 SJ=XMAX-(K-1)*(XMAX-XMIN)/50.
64 WRITE(6,20)SJ
65
66 WRITE(6,21)
67 IF(K=50)4,14,4
68 DO 11 J=1,101
69 L(J)=IS(1)
70 WRITE(6,25)
71 WRITE(6,20)XMIN
72 CONTINUE
73 WRITE(6,23)
74 DO 12 J=1,6
75
76 A(J)=T0+(J-1)*(TF-T0)/5.
77 WRITE(6,24)(A(J),J=1,6)
78 RETURN
79 END
80
81 SUBROUTINE MIMAX(V,VMIN,VMAX,N)
82 DIMENSION V(100)
83 VMAX=V(1)
84 VMIN=V(1)
85 DO 1 I=2,N
86 IF(V(I)-VMAX)>2.2,3
87 VMAX=V(I)
88 GO TO 1
89 2 IF(VMIN-V(I))1,1,4
90 VMIN=V(I)
91 CONTINUE
92 RETURN
93 END
94
95 $SET OWN
96
97 SUBROUTINE ASIL(IAL)
98
99 REAL KAPA,INTER,LX(24),LY(24),LZ(24),KSS(8)
100 INTEGER C1,C2,SL,TII,TN1,PARA,FSIGN,FJUMP,TMAX,TPRUM,SEG,ZVAL(2),CC
101 1,Z,T
102
103 DIMENSION NAME(10),VERFRG(100),QUTER(5,100),IS(6),INUMA(2),DENSST(1200),PSHIFT(8),SCF(8,2),POM(60),E(60,2),PH(4,60,2),AKSSL(140),AE(60
104 2),COSTHE(200),R12(290),APHI(290),NUMA(3)
105

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```

1101 FORMAT(3F10.7)
3000 T=2
      GO TO 3004
3001 T=3
3004 TN1=T+1

C      SCF(L,T) = SCALAR OF 2H3S SETTS ANGULAR MOMENTUM L FOR TYPE T
C      DESIRED, IF NOT VALUE 1.0 SHOULD BE GIVEN
C      20 READ(S,1100) (SCF(L,T),L=1,LSST)
C      ENERGY'S AND PHASESHIFT'S ALREADY TYPE T
C      30 READ(AL,1100) ((E(I+1,T),E(I+2,T),E(I+3,T),E(I+4,T),
C      *E(I+5,T),E(I+6,T),E(I+7,T),I=1,1PH,8)
C      DO 40 L=1,LSS1
C      DO 40 I=1,1PH,8
C      40 READ(AL,1100) PH(L,I,T),PH(L,I+1,T),PH(L,I+2,T),
C      *PH(L,I+3,T),PH(L,I+4,T),PH(L,I+5,T),PH(L,I+6,T),
C      DO 50 L=1,LSS1
C      DO 50 I=1,1PH,8
C      50 PH(L,I,T)=PH(L,I,T)*SCF(L,T)
C      IF(TN.EQ.T) GO TO 59
C      READ(AL,76,END=59) FMTH,FINT
C      76 FORMAT(4F10.5,215)
C      WRITE(6,6664) ENT1
C      IF(FINT1.NE.0.0) FINT=FINT1
C      IF(EINT1.NE.0.0) EINT=EINT1
C      EMIN=EINT+(0.1*EDELTA)
C      BACKSPACE IAL
59 CONTINUE

1200 WRITE(6,700) EMIN,EMAX,EDELTA
1200 FORMAT(//,PHASESHIFT USED IN CALCULATION WITH SSCF= ',F8.5)
      WRITE(6,1200) SCF(1,TN)
      IF(LSS1.GT.1) WRITE(6,1300) SCF(2,TN)
      NUMACTN=ENDMACTN/1NUMACTN
      WRITE(6,505) T,ZVAL(TN),NUMACTN
505 FORMAT(//, ATOMS TYPE,I,I : VALENCE ELECTRONS=',I3,10X,' NUMBER
      10F ATOMS=' I3/ ,ENERGIES AND PHASESHIFTS:T/')
1300 FORMAT(5X,'PSCF',5X,'PSCF',5X)
1400 FORMAT(5X,'ENERGY',5X,'S',5X,'ENERGY',7X,'P')
1488 FORMAT(1H+T49, 'ENERGY',7X,'D')
      WRITE(6,1488)
      TFLSS=GT1)WRITE(6,1488)
1500 FORMAT(2F11.5)
      D3.61 T=1,1PH
      61 WRITE(6,1500)(E(I,TN),PH(L,I,TN),L=1,LSS)
      IF(TN.EQ.T) GO TO 3002
      IF(TN=2)3000,3001,3002
3002 ELASTEFIT1
      DELIST(1)=0.0
      IF(NLIST(1)>0.0)SH PUNCH CALL PUNCH(PARA,IAL)
      LSSELS2
      62 N1=NMSC*(LSS*LSS-3)
      IF(IOPL.EQ.1)N1=N1+3.0*NMSC
      DELTAS=0.0
      CHE=U
      OLDE=EDELTA
      KE1

      FJUMP=0
      DO 3600 I=1,NUMSC
      LX(I)=AU*LX(I)
      LY(I)=AU*LY(I)
3600 LZ(I)=AU*LZ(I)
      WRITE(6,3500)(LX(I),LY(I),LZ(I),I=1,NUMSC)
3501 FORMAT(//,LX,F19.5,LY,F12.5,LZ,F12.5,T=1,1PH)
      CALL ANGLE(CL,LY,LZ,NUMSC,COSTHE,R12,APHI)
      ENERGY=EMIN
      4000 ENERGY=ENERGY-0.1*OLDEL
      IF(ENERGY.LESH TOO BROAD CHANGE THIS STEP TO SMALLER VALUE, SEE
      LABELS 4000, 4001, 123, 4002, 4003, 333, 4005 AND 949
      BEGIN CALCULATION
      WRITE(7,4001)
      4001 FORMAT(1H1,BEGIN CALCULATION)
      NCOUNT=1
      99 IF(ENERGY.GT.EMAX) GO TO 998
      KAPA=SQRT(ENERGY)
      J=0
      DO 80 L=1,LSS1
      IF(IOPL.EQ.1) GO TO 80
      IF(L.EQ.2) GO TO 80
      80 KKK=2*(L-1)+1
      DO 3005 KKK=1,KK

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```

DO 3005 TN=1,3
IF (LT,GT,T)GO TO 3005
C   CALCULATION OF K-MATRICES
DO 90 I=1,NPH
AE(I)=F(I,TD)
90 POM(I)=PH(L,I,T)
PSHIFT(L)=T*TDF(DJ,AE,UPL,ENERGY,WPP)
KSS(L)=-(STL(PSHIFT(L))/COS(PSHIFT(L)))/KAPA
I=NUMA(TN)
DO 3005 KXYZ=1,1
JE=J+1
AKSS(J)=KSS(L)
3005 CONTINUE
LMIN=1
LMIN=7,1700,LMIN1,PSHFT(L),KSS(L)
1700 FORMAT(//,1700)LMIN1 FOR L=1,T3,' SINGLE SITE PHASESHIFT='F8.5,
1' K-MATRIX='F8.5)
80 CONTINUE
C   CONSTRUCTION OF DETERMINANT
CALL GMTRIX
CDDET=DETC(G,'1')
1800 FORMAT(' REAL PART OF DET='F8.5,SX,'IMAG PART DET',F8.5)
4 WRITE(7,1800)CDDET
C***★ CALCULATION OF THE IMAGINARY PART OF LOG(DET)
2 DETRE=REAL(CDET)
3 DETIM=AIMAG(CDET)
IF (DETRE) 180,180,170
120 IF (DETIM) 140,150,130
130 FRSUM=0.5*PI
GOTO 180
140 FRSUM=1.5*PI
GOTO 180
150 FRSUM=0.0
GOTO 180
160 FRSUM=ATAN(CDETIM/DETRE)
FRSUM=FRSUM+PI
GOTO 180
170 FRSUM=ATAN(CDETIM/DETRE)
180 FRSUM=FRSUM
1900 FORMAT(' FOR ENERGY='F8.5,' RYDBERGS')
WRITE(7,1900)ENERGY
IF (K,EO,190) TO 190
DELTAS=FRSUM1-FRSUM
FSIGN=-SIGN(1.0*DELTAS)
IF (ABS(DELTAS)>T4)DELTAS=DELTAS+FSIGN*2.0*PI
200 DENSST(K)=DELTAS*2.0/(PI*DELTAS)
2000 FORMAT(' CHANGE IN DENSITY OF STATES IS ',F20.5)
WRITE(7,2000)DENSST(K)
DEST=(DENSST(K)*100.*ATOCEL/((AO**3)*NUMSC))+100*(SQRT(ENERGY)/(2*1PI*PI))
IF (DELTAS.GT.0.5*ULDFL*UR_DEST.GT.0.0)GO TO 190
TFC(SFG+(TIME(2)/760).GT.TMAX)GO TO 190
NCOUNT=NCOUNT+1
ENER=ENERGY-DELTAS
EDELTA=EDELTA/FLOAT(NCOUNT)
ENERGY=ENER+EDELTA
IF (NCOUNT.EQ.4)GO TO 190
GO TO 99
190 IF (NCOUNT.GT.1)NCOUNT=1
VENERG(K)=ENERGY
2100 FORMAT(' DENSITY OF STATES PER UNIT VOLUME*100 IS ',F20.5)
WRITE(7,2100)DEST
TIMEPO=TIME(2)/760
WRITE(7,2200)TIMEPO
2200 FORMAT('UX, /* PROCESS TIME='F8.4,' SECONDS **')
ELAST=ENERGY
IF (K,EO,99) GO TO 999
TPROMETIMEPO/K
SEG=TPROM+19
IF (SEG>TIMEPO.GT.TMAX) GO TO 999
OFRSUM=FRSUM
IF (2*(K/2).NE.K) GO TO 123
4001 EDELTA=ODEL*0.9
GO TO 124
123 EDELTA=ODEL*0.1
124 COUNT=1
K=K+1
ENERGY=ENERGY+EDELTA
GOTO 99
998 KEK=1
999 CC =NUMA(1)*ZVAL(1)+NUMC(2)*ZVAL(2)

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FEL=0.9
2400 FORMAT(1H//10X,'INTEGRATED CHARGE',10X,'FPEF',10X,'DENSITY',10X,'INTE
1GRENED DENSITY OF STATES')
10X,'DEMS OF STATES') 01242000
01243000
01244000
01245000
01246000
01247000
01248000
01249000
01250000
01251000
01252000
01253000
01254000
01255000
01256000
01257000
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01262000
01263000
01264000
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01308000
01309000
01310000
01311000
01312000
01313000
01314000
01315000
01316000
01317000
01318000
01319000
01320000
01321000
01322000
01323000
01324000
01325000
C4002 WRITE(6,2400)
ENERGY=EMIN-0.9*OLDEL-0.1*OLDEL
DU 210 I=1,K
IF(2*(I/2).NE.I) GO TO 333
C4003 EDELTA=OLDEL*0.1
GO TO 334
C 333 EDELTA=OLDEL*0.9
CONTINUE
C ENERGY=ENERGY+EDELTA
ENERGY=VENERG(I)
QINTER(1,I)=(A0**3)*SQRT(ENERGY)*NUMSC/(2.0*ATOCCEL*PI*PI)
QINTER(2,I)=QINTER(1,I)+DENST(I)
IF(2*(I/2).NE.I.OR.FEL.NE.0.0) GO TO 210
ENI=ENERGY
FINT=QINTER(2,I)*ENI+FINT
ENI=ENERGY
IF(FINT-CC)210,335,335
335 WRITE(6,2401)
FEL=ENERGY
2401 FORMAT(1H//10X,'FERMI LEVEL')
210 WRITE(6,2500) ENERGY,DENST(I),QINTER(1,I),QINTER(2,I),FINT
2600 FORMAT(10X,'ENERGY',10X,'DENST(I)',10X,'FRIEDEL SUM',8X,'100*N(E)/VOLUME')
2500 FORMAT(1H//SF20.5)
C4004 ENERGY=EMIN-1.0*OLDEL
DO 4004 I=1,K
IF(2*(I/2).NE.I) GO TO 4004
QINTER(P,I)=QINTER(2,I+1)
4004 CONTINUE
CALL CARTEK(QINTER,VENERG,IS,2,FEL)
WRITE(6,2600)
DU 220 I=1,K
IF(2*(I/2).NE.I) GO TO 949
C4005 EDELTA=OLDEL*0.1
GO TO 950
C 949 EDELTA=OLDEL*0.9
950 CONTINUE
ENERGY= VENERG(I)
C ENERGY=ENERGY+EDELTA
DENST(I)=DENST(I)*100.0*ATOCCEL/((A0**3)*NUMSC)
PINTER=DENST(I)*(SQR(ENERGY)/(2*PI**2))*100
IF(2*(I/2).NE.I) PITE(0,2500) ENERGY,DENST(I),RINTER
TF(2*(I/2).NE.I) PITE(0,2500) ENERGY,DENST(I),RINTER
220 CONTINUE
C IF(ENERGY+OLDEL.LT.EMAX) GO TO 621
IALE0
RETURN
C INTEGRATED DENSITY OF STATES NOT USED
A INTEGRATION IS MADE WHEN REQUIRED
2501 FORMAT(SF20.5,1)
C IF NEW CONFIGURATION WANTED FOR SAME SCATTERERS
READ(5,1100)(LX(I))(LY(I),LZ(I)),I=1,NUMSC
XXX=(LX(1)-LX(2))*(LX(1)-LX(2)),I=1,NUMSC
YYY=(LY(1)-LY(2))*(LY(1)-LY(2))
ZZZ=(LZ(1)-LZ(2))*(LZ(1)-LZ(2))
RXYZ=XXX*YYY*ZZZ
IF(RXYZ.EQ.0.0) GO TO 620
GO TO 621
621 WRITE(6,2601)
IF(IAL.NE.5) PITE(IAL,0665) ELAST,FINT
6665 FORMAT(2E10.7)
IF(IAL.NE.5)LOCK IAL
IF(NAME(10).EQ.'H' .LOCK), GO TO 622
66 FORMAT(1H//10X,5('*'),1H//10X,'WORK ENDED BECAUSE TIME IS NEARLY UP')
WRITE(6,6666) TIE,PU,PLAST
6666 FORMAT(1H//10X,'TOTAL PROCESS TIME='F10.5,9X,'LAST ENERGY ACCOUNTED
6664 *='F10.7),1H//10X,'ENERGY REGION FROM EMIN TO ',F10.7,' HAS BE
*EN ALREADY CALCULATED IN PREVIOUS JOB'//110('*'))
C 620 CONTINUE
IALE0
RETURN
SPESET Q/N
END

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SUBROUTINE GMTRIX
REAL KAPA,LX(24),LY(24),LZ(24),KSS(8),NL,JL
INTEGER C1,C2,SU,FSHIFT,E
DIMENSTON AKSS(14),PSHIFT(8),SCF(8,2),E(60,2),POM(60),PH(4,60,2),
1COSTHE(290),R12(290),APHI(290)
COMPLEX KSC(20,4),PUTC(20),KAPC,ENERGC,BTH(20),VHTH,YC,CONDET,C(14
16,140),AUC,SUC1,SUC2,APC,S2C1,S2C2,ZERO

COMMON/VCOMPL/G,KSC,KAPC,LHEPGC,PUTC
COMMON/VARRE/LX,LY,LZ,KSS,PSHIFT,SCF,E,POM,PH,AKSS,COSTHE,R12,APHI
COMMON/VSIMP/KAPA,DETRE,DETRIN,DEFSUN,PI,ENERGY,FSIGN,FJUMP,N1,NE,L
1SS1,NUMSC,TDPL

399 ZERO=CMPLX(0.0,1.0)
LSS=LSS-1
DO 10 J=1,M1
DO 10 J=1,M1
10 G(I,J)=CMPLX(0.0,0.0)
C1=0
C2=0
CONST=4.0*PI*KAPA
L1=0
21 CONTINUE
IF(L1.EQ.1.AND.IOPL.NE.1) GO TO 23
M1=-1
22 CONTINUE
L2=L1
31 CONTINUE
IF(IOP1.EQ.1) GO TO 801
IF(L2.EQ.1) GO TO 400
301 IF(L2.EQ.L1) M1=-L2
LMAX=L1+L2
LMIN=L2-L1
M2=M1
41 DO 50 I=1,NUMSC
J1=
IF((M1.EQ.M2).AND.(L1.EQ.L2)) J1=I+1
IF(J1.GT.NUMSC) GOTO 50
DO 50 J=J1,NUMSC
J1=
IF(J.EQ.1) GOTO 100
IF(J.GT.1) GOTO 101
KK=(J-1)*NUMSC+I-J*(J+1)/2
RER12(KK)
THETA=COSTHE(KK)
IFI=APHI(KK)+PI
GO TO 102
101 KK=J-I+(I-1)*NUMSC-(I*I-I)/2
RER12(KK)
THETA=COSTHE(KK)
IFI=APHI(KK)
102 CONTINUE
1090 R1=KAPA*R
299 S2C1=CMPLX(0.0,0.0)
399 S2C2=S2C1
499 SUC1=S2C1
599 SUC2=SUC1
L3=MIN
72 CONTINUE
M3=I*L3
71 X=L2,M2,L1,I1,L3,M3)
AUX=(L1,M1,L2,M2,L3,M3)
IF(ABS(X).LT.1.001) GOTO 1699
699 AUC=YC(L3,I3,THETA,FI)*C0*ST*X
5 SUC1=SUC1+YL(L3,I3)*AUC*(ZER0)**L3
5 SUC2=SUC2+YL(L3,I3)*AUC*(ZER0)**L3
1699 IF(ABS(AUX).LT.1.001) GOTO 73
AUC=YC(L3,I3,THETA,FI)*C0*ST*AUX
3 S2C1=S2C1+YL(L3,I3)*AUC*(ZER0)**L3
4 S2C2=S2C2+YL(L3,I3)*AUC*(ZER0)**L3
73 CONTINUE

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```

N3=L3+1
IF(L3.GT.L3) GOTO 31
GOTO 71
L3=L3+1
IF(L3.GT.LMAXJ) GOTO 70
GOTO 72
70 CONTINUE
IC1=C1+I
JC2=C2+J
5 G(JC1,JC2)=-SUC1+SUC2*ZERO
6 G(JC2,IC1)=-S2C1+S2C2*ZERO
100 CONTINUE
60 CONTINUE
50 CONTINUE
C2=C2+NUMSC
M2=M2+1
IF(M2.GT.L2)GOTO 40
GOTO 41
40 CONTINUE
L2=L2+1
IF(L2.GT.LSS)GOTO 24
GOTO 31
24 CONTINUE
CONTINUE
C1=C1+NUMSC
C2=C1
M1=M1+1
IF(M1.GT.L1) GOTO 23
GOTO 22
23 L1=L1+1
IF(L1.GT.LSS)GOTO 20
GOTO 21
20 CONTINUE
DO 90 I=1,M1
90 G(I,I)= KAPA*ZERO
DO 120 J=1,M1
120 G(I,J)=G(I,J)*AKSS(J)
DO 130 I=1,M1
130 G(I,I)=I*G(I,I)
2500 FORMAT(/3X,10F11.4)
2501 FORMAT(6I4,2F8.4)
130 CONTINUE
RETURN
END

COMPLEX FUNCTION YC(L,N,CTH,PH)
***** EVALUATES COMPLEX SPHERICAL HARMONICS Y(L,M), CTH=COS(THETA)
***** PH=PHI
M=N
Z=(2.0*L+1.0)/12.5603753
1000 A=1.0
B=-1.0
M=-M
C=M*PH
Z=Z*F(L-M)/F(L+M)
IF (Z) 1070,1090,1100
1070 Z=SQRT(-1.0*Z)*P(L,0,CTH)
1090 YC=CMPLX(0.0,Z)
1100 RETURN
1040 Z=Z*SORT(Z)*P(L,0,CTH)
1050 YC=CMPLX(Z,0.0)
1060 RETURN
A=(-1.0)**M
B=A
C=-PH
Z=Z*F(L-M)/F(L+M)
IF (Z) 1070,1090,1100
1070 Z=SQRT(-1.0*Z)*P(L,M,CTH)
X=Z*ASIN(C)*A
Y=Z*ACOS(C)*B
1080 Y=CMPLX(X,Y)
1090 Y=CMPLX(0.0,0.0)
1100 Z=SQRT(Z)*P(L,M,CTH)
X=Z*COS(C)*A
Y=Z*STN(C)*B
1110 Y=CMPLX(X,Y)
1120 RETURN
END

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SUBROUTINE ANGLE(LX,LY,LZ,NUMSC,COSTHE,APHI)
REAL COSTHE(299),LY(299),APHI(299)
REAL LY(24),LY(24),Z(24)
K=1
PI=3.141593

DO 50 I=1,NUMSC
J1=I+1
IF(J1.GT.NUMSC) GOTO 50
DO 60 J=J1,NUMSC
RX=LX(I)-LX(J)
RY=LY(I)-LY(J)
RZ=LZ(I)-LZ(J)
RESORT(RX*RX+RY*RY+RZ*RZ)
IF(RX) 1010,1040,1050
1010 IF(RY) 1020,1030,1030
1020 FI=ATAN(RY/RX)-PI
GOTO 1090
1030 FI=ATAN(RY/RX)+PI
GOTO 1090
1040 IF(RY) 1050,1060,1070
1050 FI=0.5*PI
GOTO 1090
1060 FI=0
GOTO 1090
1070 FI=0.5*PI
GOTO 1090
1080 FI=ATAN(RY/RX)
1090 CONTINUE
THETA=RZ/R
R12(K)=R
COSTHE(K)=THETA
APHI(K)=FI
K=K+1
60 CONTINUE
50 CONTINUE
RETURN
END

REAL FUNCTION NL(L,R)
**** TO EVALUATE SPHERICAL NEUMANN FUNCTIONS
NL=-1.0E60
IF(R)20,10,20
10 WRITE(6,1)L
1 FORMAT(//,I1) ERROR IN SPHERICAL NEUMANN FUNCTION R=J L=I,I4)
GOTO 105
20 IF(L)40,30,40
30 NLE=-COS(P)/R
GOTO 105
**** COMPUTATION OF SUM
40 AE1=0
SUM=1.0
NT=1
50 A=-[R**R/(2*INT*(2*JT-1-2*L)))*A
SUM=SUM+A
NT=NT+1
RI=ABS(A/SUM)
IF(RI.LT.1.0E-6) GOTO 80
60 IF(JT>150)70,60
60 WRITE(6,2)L,JT,60
2 FORMAT(//,I1,I4,I1,F12.6)
1 TERMS L=I,I4 , I R= F12.6)
70 CONTINUE
GOTO 80
80 L1=2*L-1

NLE=DF(L1)*SUM/(R***(L+1))
100 CONTINUE
RETURN
END

REAL FUNCTION JL(L,R)
**** CALCULATES BESSEL FUNCTIONS OF ORDER L AND ARGUMENT R
IF(R)20,10,5
10 IF(L.EQ.0) JL=1.0
IF(L.GT.0) JL=0.0
GOTO 10
20 L1=2*L+1
A=(R**L)/DF(L1)
K=1
SUM=A
30 A=-R**R/(2.0*INT(K+2.0*L+1.0)*K)*A
SUM=SUM+A
IF(CABS(SUM/LT.1.0E-6)) GOTO 40
K=K+1

```

```

IF(K.LF.150) GOTO 30
WRITE(6,1)L,P
1 FORMAT(//) L,SERIES FOR SPHERICAL BESSEL FUNCTION DID NOT CONVERGE
1AFTER 150 TER IS L= 'I,I4,' R= ',F12.6)
GOTO 40
40 JLESUM
100 CONTINUE
RETURN
END

FUNCTION P(N,M,X)
C*** THIS FUNCTION EVALUATES ASSOCIATED LEGENDRE POLYNOMIALS OF
C*** ORDER (N,M) ARGUMENT X
C*** TREAT SPECIAL CASES
IF((N>20,10,20
10 P=1.0
GOTO 100
20 IF(X)>0.22,50
22 RI=(N-M)/2
23 PI=(N-M)/3
RI=ABS(RI-PI)
IF(RI.GT.0.002) GOTO 30
GOTO 40
30 P=0.0
GOTO 100
40 T=(-1)**((N-M)/2)
P=T*DF(N+M-1)/DF(N-M)
GOTO 100
50 IF((1-ABS(X))>0.001) GOTO 70
60 IF(N.EQ.0) P=X**N
IF(N.NE.0) P=0.0
GOTO 100
70 CONTINUE
C*** NOW TO COMPUTE GENERAL CASE
N1=2*N-1
NM=N-1
IF(NM)90,80,90
80 SUM=DF(N1)
GOTO 100
90 P=DF(N1)*(X**(N-M))/F(NM)
SUM=P
IF(NM.EQ.1) GOTO 100
KM=NM/2
DO 110 K=1,KM
T1=2.0*K-2.0*K+1.0
T2=NM-2.0*K+1.0
T3=NM-2.0*K-1.0
B=-((T2*T3)/(2.0*X*X*T1*K))*B
110 SUM=SUM+B
1000 X1=1.0-X*X
R2=FLOAT(M)/2.0*ALOG(X1)
P2=EXP(R2)*SUM
100 CONTINUE
RETURN
END

COMPLEX FUNCTION DETC(A,N)
COMPLEX A(140,140)
C*** EVALUATES THE DETERMINANT OF A COMPLEX MATRIX WITH ROW PIVOTING
C*** BEGIN COMPUTATION OF DET
4 DETC=CMLPX(1.0,0.0)
DO 10 I=1,N
1 PIVOT=CAPS(A(I,I))*(CABS(A(1,1)))
KEI
C*** LOOK FOR PIVOT ELEMENT
11 I=I+1
IF(I>N) GO TO 50
DO 20 J=I,N
2 RK=REAL(A(J,I))
3 PI=AIMAG(A(J,I))
AV=RK*RK+PI*PI
IF(PIVOT-AV) 30,20,20
30 PIVOT=AV
KEJ
20 CONTINUE
C*** K IS THE ROW WITH THE LARGEST ELEMENT
C*** INTERCHANGE ROWS
4 IF(K-I) 40,50,40
40 DO 60 J=1,N
5 T=A(I,J)
6 A(I,J)=A(K,J)
60 A(K,J)=T

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```

C**** 7 DETC=DETC
      END INTCHANGE ROWS
      50 CONTINUE
      55 RK=REAL(A(I,I))
      60 PI=ATAN2(A(1,1))
      65 IE(RK)80,70,80
      70 IF(RK)80,100,80
1000 DETC=CMLX(U,S,V)
      GOTO 1020
     80 CONTINUE
C**** MULTIPLY ROW I BY -A(I,J)/A(I,I) AND ADD IT TO ROW J
     85 I=I+1
     86 IF(I>J) GO TO 100
     87 DO 90 J=1,I
     88 W=-A(J,I)/A(I,I)
     89 DO 100 L=1,I
     90 A(J,L)=A(J,L)+W*A(I,L)
     91 CONTINUE
     92 DO 110 I=1,N
     93 DETC=DETC*A(I,I)/CABS(A(I,I))
1000 CONTINUE
      RETURN
END

FUNCTION C(LT1,MT1,LT2,MT2,LT3,MT3)
COMPUTES THE GAUSS NUMBERS
INTEGER S
C**** CHECK GENERAL CONDITIONS
LT1=LT3
MT1=MT3
LT2=LT3
MT2=MT3
LT3=LT1
MT3=MT1
LT=LT1+2+LT3
RL=FLUT(LT/2)*2.0
RL1=LT1+2+LT3
IF(RL-RL1)10,20,10
10 C=0.0
GOTO 100
20 IF((IABS(M1).GT.L1).OR.(IABS(M2).GT.L2).OR.(IABS(M3).GT.L3))
   1 GO TO 10
   L12=L1+L2
   L11=IABS(L1-L2)
   L23=L2+L3
   L22=IABS(L3-L2)
   M22=M2+M1
   L13=L1+L3
   L33=IABS(L1-L3)
   TF=(L3.GT.L12).OR.(L3.LT.-L11)) GOTO 10
   TF=(L1.GT.L23).OR.(L1.LT.-L22)) GOTO 10
   TF=(L3.GT.L13).OR.(L3.LT.-L23)) GOTO 10
C**** REARRANGEMENT OF THE M
LT=(1+LT+LT)/2
COEF1=SQRT(F(2*LT-2*L1)*F(2*LT-2*L2)*F(2*LT-2*L3)/F(2*LT+1))*(-1)**(L1-L2
1+LT)
COEF2=SQRT(F(2*LT-2*L1)*F(2*LT-2*L2)*F(2*LT-2*L3)/F(2*LT+1))*(-1)**(L1-L2
1+LT+LT)
COEF3=SQRT(F(L1+L2+L3)*F(L1-M1)*F(L2-M2)*F(L3-M3)*F(L3+M3)/
1(F(2*LT+1)*F(L1+L2+L3)*F(L2+L3-L1)*F(L1+M1)*F(L2+M2)))
S=0
FF=0.0
30 F1=(-1)**(S+L1-M1)
MT=L1-M1-S
IF(MT.LT.0) GOTO 40
F2=F(MT)
MT=L3-M3-S
IE(MT-LT,0) GOTO 40
IF(-(L3+L1+M1)*F(L1+M1+S)*F(L2+L3-M1-S)*F1/(F(S)*
1F2+F(MT)*F(L2+L3+M1+S)) FF=FF+F(L1+M1+S)*F(L2+L3-M1-S)*F1/(F(S)*
S=S+1
GOTO 30
40 C=COEF1*COEF2*COEF3*FF
100 CONTINUE
      RETURN
END

FUNCTION F(N)
FACTORIAL
IF(N)10,20,30
10 F=0.0
GOTO 100

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20 F=1.0          01743000
30 GOTO 100      01744000
40 IF(N.LT.2) GOTO 50 01745000
40 DO 40 L=3,10 01746000
40 DF=L*RF      01748000
50 F=RF          01749000
100 RETURN        01750000
END             01751000
FUNCTION DF()    01752000
C**** DF=DOUBLE FACTORIAL OF N 01753000
IF(N>10,20,30) 01754000
10 DF=0.0         01755000
20 GOTO 100      01756000
30 DF=1.0         01757000
GOTO 100         01758000
30 RN=N/2.0       01759000
PI=N/2.0         01760000
IF(RN.EQ.RT) GOTO 50 01761000
TE=1.0           01762000
DO 40 K=1,N,2   01763000
40 TET*K        01764000
DF=T            01765000
GOTO 100         01766000
50 TE=1.0         01767000
IF(TE.LT.?) GOTO 70 01768000
DO 60 K=2,N,2   01769000
60 TET*K        01770000
70 DFET          01771000
100 RETURN        01772000
END             01773000
COMPLEX FUNCTION RL(L,R) 01774000
REAL JL, JR     01775000
AH=JL(L,R)
BH=JR(L,R)
HE=COMPLEX(AH,BH)
RETURN          01776000
END             01777000
SUBROUTINE RESIS(COMEGA,VFERMI,Z,DELELE,N) 01778000
C*** OMEGA = VOLUMEN ATOMICO, SIGMA = DIAMETRO DE ESFERAS. 01779000
C*** DELELE = CORPIGIENTES DE FASE, KFERMI = VECTOR DE FERMI. 01780000
C*** VFERMI = ENERGIA DEL NIVEL DE FERMI; VFERMI = VELOCIDAD DE FERMI. 01781000
C*** AQUUP, XAQUUP = TABLA DEL FACTOR DE ESTRUCTURA; POT = POTENCIAL. 01782000
C*** PACFRM = EMPAQUETAMIENTO; TSO = MATRIZ DE TRANSICION. 01783000
C*** VINTEG = VALOR DE LA INTEGRAL; RH0(I) = RESISTIVIDAD. 01784000
C*** KFERMI VALF SORT (FERMI EN 17METROS) 01785000
DIMENSION C(9), AQUUP(40), DELELE(40), XAQUUP(40), 01786000
%SIGMA(9), RH0(9), VECFER(9), PACFRM(9) 01787000
REAL INTER      01788000
REAL KFERMI, KFERMO, M 01789000
CE=1.0           01790000
PT=4.14592654  01791000
SIGMA=((3.5/4.)*(0.5+0.15)/PI)**(1./3.)**2 01792000
CUNTRAS=21.74444430 01793000
53 READ(5,130) (AQUUP(J), J=1,40) 01794000
DO 1 KL=1,40 01795000
1 XAQUUP(KL)=1./Z.*KL 01796000
60 WRITE(6,200) 01797000
61 WRITE(6,210) 01798000
70 WRITE(6,220) 01799000
75 WRITE(6,230) 01800000
63 WRITE(6,240) (DELELE(K),K=1,4) 01801000
63 WRITE(6,230) (DELELE(K),K=1,4) 01802000
I=0              01803000
KFERMI=SORT(CFERMI) 01804000
KFERMO=KFERMI 01805000
64 WRITE(6,240) 01806000
2 I=I+1          01807000
M=6.0            01808000
SUMA1=0.0         01809000
SUMA2=0.0         01810000
OULD=0.0          01811000
VINTEG=0.0         01812000
TETHA=0.0          01813000
SIGM(I)=SIGMA 01814000
VFERMI=CF*KFERMI 01815000
C(I)=3.*(PT**2)*(OMEGA*KFERMI)**2 01816000
PACFRM(I)=4.*3.141592653589793/(24.*OMEGA) 01817000
3 TETHA=TETHA+PI/180. 01818000
X=COS(TETHA) 01819000
PI=1. 01820000

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P2=X
P4EJ=5*(3.*X**2-1./)
P4EJ=5*(5.*X**3-3.-4.)
P5EJ=125*(35.*X**4-32.*X**2+3.)
SUMA1=S1*(DELELE(1))+COS(DELELE(1))+3.*P2*SIN(DELELE(2))*COS
(%(DELELE(2))+5.*P3*X*31*(DELELE(3))+COS(DELELE(3))+7.*P4*SIN(DELELE(4
%))*COS(DELELE(4))
SUMA2=P1*(S1*(DELELE(1))**2+3.*P2*(SIN(DELELE(2))**2)+5.*P3
%*(SIN(DELELE(3))**2)+7.*P4*(SIN(DELELE(4))**2)
QDLD=0
TS0=SUMA1**2+S1*2*2**2
POTEN=SQRT(TS0)
DEKFER=M*SQRT(2.*((1-X)))
AQ=INTER(AQUP,XAUP,40,3*SIGMA ,10)
COSAS=AQ*3*REFERT
VINITEG=VINITEG+COSA*TISN*(D-QDLD)
IF(TETHAL=0,999*P1) GO TO 3
PH0(I)=C(I)*VINITEG
RH0(I)=CONTRA*RH0(I)
SIGMA=SIGMA-0.05*STO(I)
LSIGMA=LSIGMA+1
VECFER(I)=REFERT
IF((LSIGMA.LT.JIGU).TO 2
65 WRITE(6,254) (BACFEM(I),I=1,3)
66 WRITE(6,250) TEIP
67 WRITE(6,270)
68 WRITE(6,280) (AJUP(L),XAUP(L),L=1,40)
69 WRITE(6,801)
72 WRITE(6,800) (SIG I(M),VECFER(M),RHO(M),M=1,9)
73 WRITE(6,330)

FORMATOS DE LECTURA E IMPRESION
30 FORMAT(8F10.5)
31 FORMAT(1H1,/,3Fx,"")
19 FORMAT(1H1,/,3Fx,"")          CALCULO DE LA RESISTIVIDAD DE METALE
18 FORMAT(1H1,/,40X,"")          "ENERGIA DEL NIVEL DE FERMI",20X,"V
19 FORMAT(1H1,/,40X,"")          "VOLUMEN ATOMICO",1X
20 FORMAT(21X,"      ",5X,F12.10,32X,F10.5)
30 FORMAT(7/5X,"CORRIENTE EN LA FASE",5X,"DELTA(S)=",F9.6,2X,"DELTA(P
%)=",F9.6,2X,"DELTA(C)=",F9.6,2X,"DELTA(F)=",F9.6,2X)
40 FORMAT(7/40X,"VELOCIDAD DE FERMI",15X,"CONSTANTE")
50 FORMAT(7/42X,"AMPERES",15X,"")
54 FORMAT(7/20X,"AMPORACIONES",15X,"I =",F10.8,8X,"II =",F10.8,8X
%"III =",F10.8)
60 FORMAT(7/25X,"TABLA DE VALORES DEL FACTOR DE ESTRUCTURA A T =",I4
%" GRADOS CENT.",1)
70 FORMAT(10X,5"(AJUP",5X,"XAUP",7X))
80 FORMAT(7/8X,F0.3,2X,F0.3,5X"/"))
90 FOPEN(7/3X,"MATERIAL",10X,3X,"POTENCIAL",8X,"3X,"DIAMETRO DE
12 LA ESFERA",3X,"VECTOR DE FERMI",5X,"INTEGRAL",8X,"3X,"RESISTIVIDADES
13 RESPECTIVAS",1X)
20 FORMAT(3X,F0.6,2X,F15.11,3X,"*",1X,F9.5,4X,"*",5X,F12.10,5X,"*",4X,
1X,F9.5,4X,"*",1X,F15.10,5X,"*",2X,F15.10,3X,"MM-CM **")
30 FORMAT(1H1,/,25X,"DIAMETRO DE LA ESFERA",10X,"VECTOR DE FERMI",13X,"R
13 RESISTIVIDADES ESPECIFICAS",1X)
40 FORMAT(21X,"*",3X,F15.10,10X,"*",3X,F15.10,6X,"*",6X,F15.10,3X,"MM
13-CM **")
50 RETURN
END
SUBROUTINE PUNCH(PARA,TAL)
DIMENSION A(2)
INTEGER PARA
REWIND 1A
1 READ(1A,2,END=3)A
2 FORMAT(20A4)
PUNCH 2,A
3 IF(PARA.GT.0) CALL EXIT
RETURN
END

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